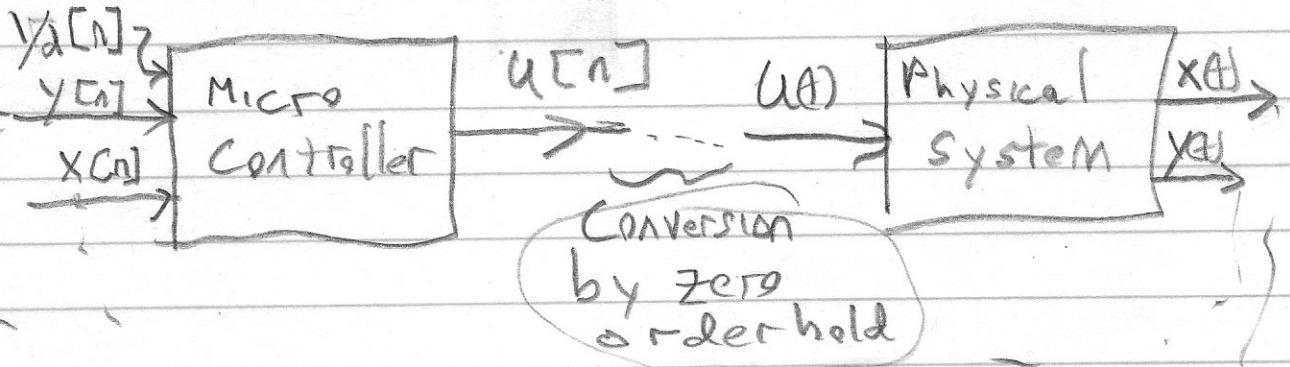


6.302

11/29/21 -> 12/1/21

(1)

# Mixed Discrete - Continuous System



CONVERSION by sampling

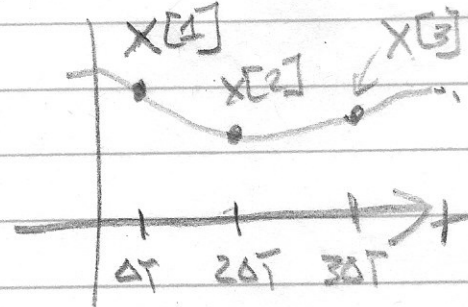
IGNORING finite # bits effect!

Sampling Analog  $\rightarrow$  Digital CONVERSION every  $\Delta T$  seconds

$$x_c[n] = x(n\Delta T)$$

$$y_c[n] = y(n\Delta T)$$

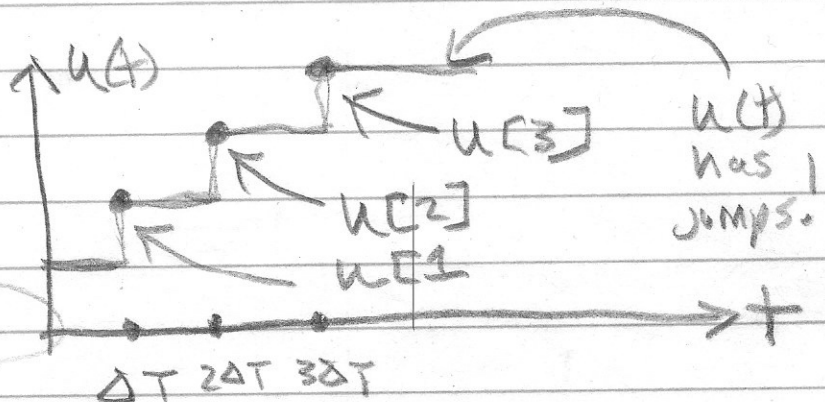
$$y_d[n] = y_d(n\Delta T)$$



## Zero Order Hold

$$u(t) = u\left(\left\lfloor \frac{t}{\Delta T} \right\rfloor\right)$$

$\lfloor x \rfloor$  = Greatest integer  $\leq x$



6.302

1A

Quick Reminder about C2b

Solution to constant input case:

Scalar Case

Vector Case

Ego

$$\frac{d}{dt} X(t) = a X(t) + b u_0$$

$$\frac{d}{dt} X = A X + B u_0$$

$$X(t) \Big|_{t=0} = X(0) \quad \text{constant}$$

$$X(t) \Big|_{t=0} = X(0)$$

Soln

$$X(t) = e^{at} X(0) + (e^{at} - 1) \frac{b}{a} u_0$$

$$X(t) = e^{At} X(0)$$

$$+ (e^{At} - I) A^{-1} B u_0$$

Proof

$$X(t) \Big|_{t=0} = e^{a \cdot 0} X(0) + (1 - 1) \frac{b}{a} u_0$$

$$\stackrel{=1}{=} X(0) \quad \text{Matches I.C.}$$

Since  $e^{At} \Big|_{t=0} = I$

$$\frac{d}{dt} X(t) = a e^{at} X(0) + a e^{at} \frac{b}{a} u_0$$

$$X(t) \Big|_{t=0} = X(0)$$

$$= a \left( e^{at} X(0) + (e^{at} - 1) \frac{b}{a} u_0 \right)$$

$$+ b u_0 \quad X(t)$$

$$\stackrel{\checkmark}{=} a X(t) + b u_0$$

Matches D.P.P. Eqn.

Since  $\frac{d}{dt} e^{At} = A e^{At} = e^{At} A$

$$\frac{d}{dt} X(t) = A e^{At} X(0)$$

$$+ A e^{At} A^{-1} B u_0$$

$$\stackrel{\checkmark}{=} A \left( e^{At} X(0) + (e^{At} - I) A^{-1} B u_0 \right) + B u_0$$

$$e^{at} X = \left(1 + at + \frac{1}{2}(at)^2 + \frac{1}{6}(at)^3 + \dots\right) X$$

$$e^{At} \vec{X} = \left(I + At + \frac{1}{2}(At)^2 + \dots\right) \vec{X}$$

(13)

Repeating From Previous Page

Does  $X(t) = e^{at} X(0) + (e^{at} - 1) \frac{b}{a} U_0$ ?

Does  $\vec{X}(t) = e^{At} \vec{X}(0) + (e^{At} - I) A^{-1} B U_0$ ?

Solve  $\frac{d}{dt} X(t) = aX(t) + bU_0$ !

Solve  $\dot{\vec{X}}(t) = A\vec{X}(t) + B U_0$ !

IF  $a < 0$ , look at steady state

IF  $\text{Re}(\text{eig}(A)) < 0$  look at steady state

$\lim_{t \rightarrow \infty} X(t) = X(\infty) = X_{ss}$   
 ↑  
 steady state

$\lim_{t \rightarrow \infty} \vec{X}(t) = \vec{X}(\infty) = \vec{X}_{ss}$

$\frac{d}{dt} X_{ss} = aX_{ss} + bU_0$

$\frac{d}{dt} \vec{X}_{ss} = A\vec{X}_{ss} + B U_0$

$\Rightarrow X_{ss} = \frac{-b}{a} U_0$

$\Rightarrow A\vec{X}_{ss} = -B U_0$

$X(t) = e^{at} X(0) + (e^{at} - 1) \frac{b}{a} U_0$

$\vec{X}_{ss} = -A^{-1} B U_0$

$\lim_{t \rightarrow \infty} 0 \cdot X(0) + (0 - 1) \frac{b}{a} U_0$

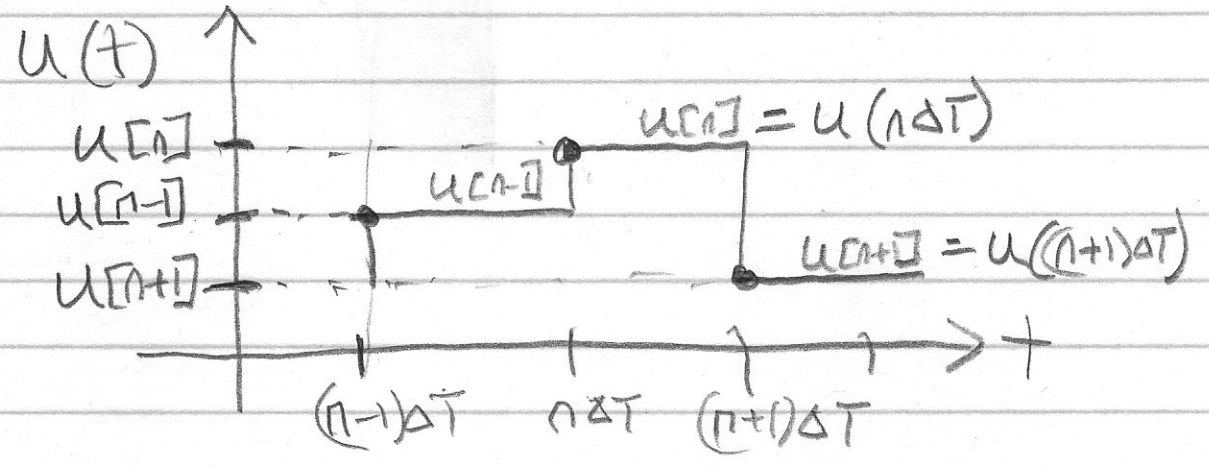
$\vec{X}(t) = e^{At} \vec{X}(0) + (e^{At} - I) A^{-1} B U_0$

$\Rightarrow X_{ss} = \frac{-b}{a} U_0$

$= 0 \cdot \vec{X}(0) + (-I) A^{-1} B U_0$   
 $= -A^{-1} B U_0$

2

# Zero-Order Hold



Let  $X(0) = X((n-1)\Delta T) = X[n-1]$ ,  $u_0 = u((n-1)\Delta T) = u[n-1]$   
 in constant input solution

## Scalar Case

$$X(n\Delta T) = e^{a\Delta T} X((n-1)\Delta T) + (e^{a\Delta T} - 1) \frac{b}{a} u((n-1)\Delta T)$$

$$X[n] = e^{a\Delta T} X[n-1] + (e^{a\Delta T} - 1) \frac{b}{a} u[n-1]$$

## Vector Case

$$X(n\Delta T) = e^{A\Delta T} X((n-1)\Delta T) + (e^{A\Delta T} - I) A^{-1} B u((n-1)\Delta T)$$

$$X[n] = e^{A\Delta T} X[n-1] + (e^{A\Delta T} - I) A^{-1} B u[n-1]$$

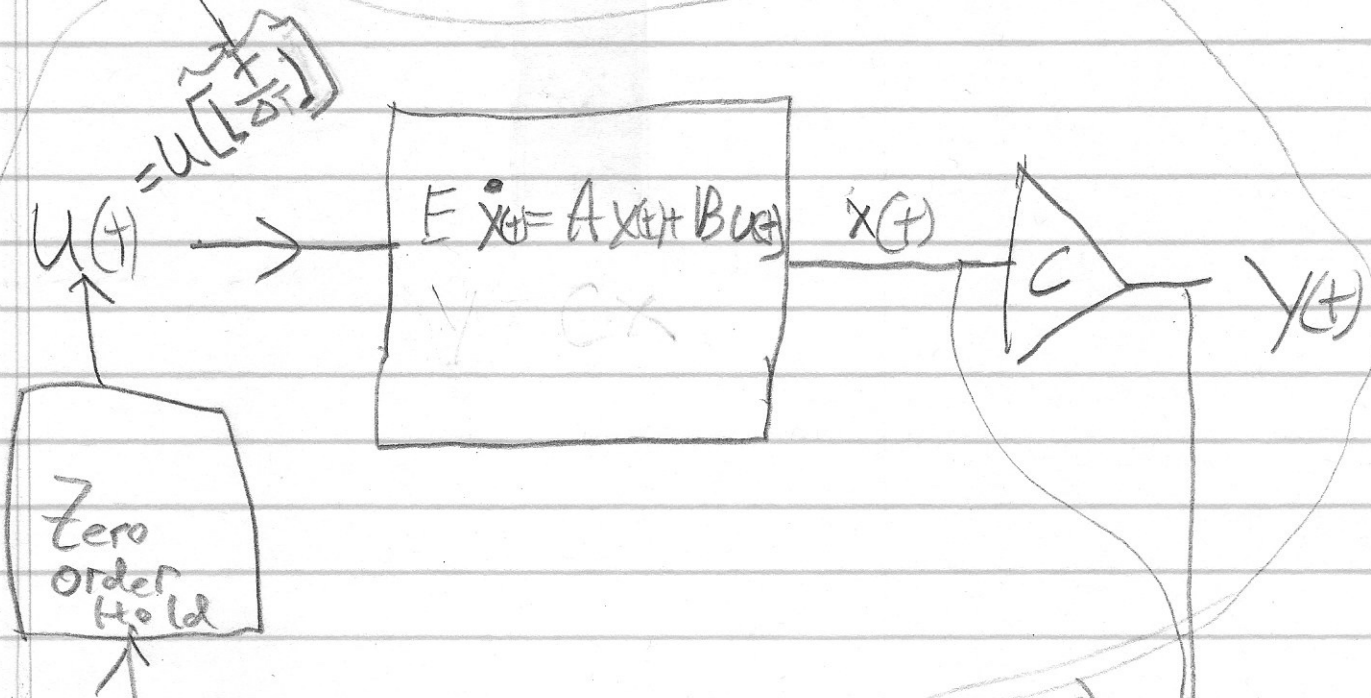
$A_d$

$B_d$

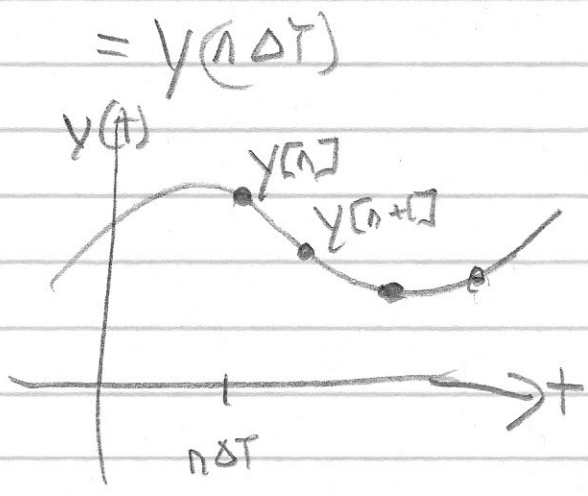
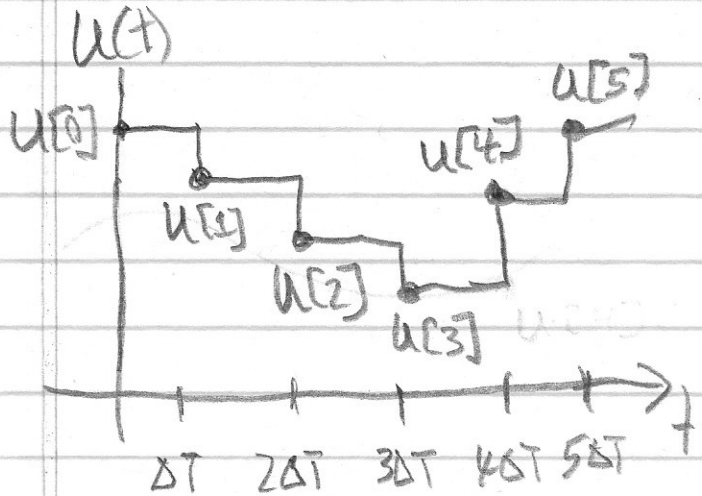
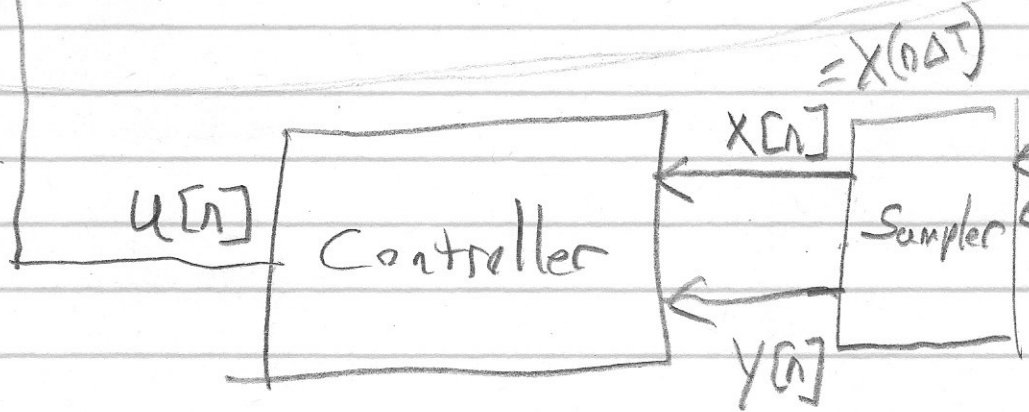
$\lfloor x \rfloor \equiv$  largest integer  $< x$

(2A)

Plant + Controller



Replace with DT System



# Discrete-Time State-Space Model

$$X[n] = A_d X[n-1] + B_d U[n-1]$$

$$Y[n] = C X[n]$$

CT & DT C's are equal!

$e^{A\Delta T}$

$(e^{A\Delta T} - I)A^{-1}B$

## State Feedback Control

$$U[n] = K_f Y_d[n] - K_d X[n]$$

## Closed-Loop System

$$X[n] = (A_d - B_d K_d) X[n-1] + B_d K_f Y_d[n-1]$$

IF  $Y_d = 0$

$$X[n] = (A_d - B_d K_d)^n X[0]$$

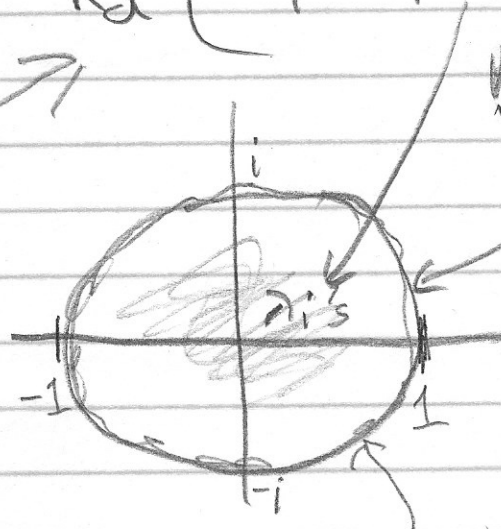
Want  $X[n] \rightarrow 0$  as fast as possible!

# Picking $K_d$

## Pole placement

$$\max_i \min_{K_d} \left( \max_i |\lambda_i(A_d - B_d K_d)| \right)$$

can be ineffective!



place  $\lambda_i$ 's well inside unit circle

UNIT circle

UNIT circle

## LQR for Discrete-Time

Pick  $K_d$  to minimize

$$\sum_{m=0}^{\infty} X^T[m] Q X[m] + u^T[m] R u[m]$$

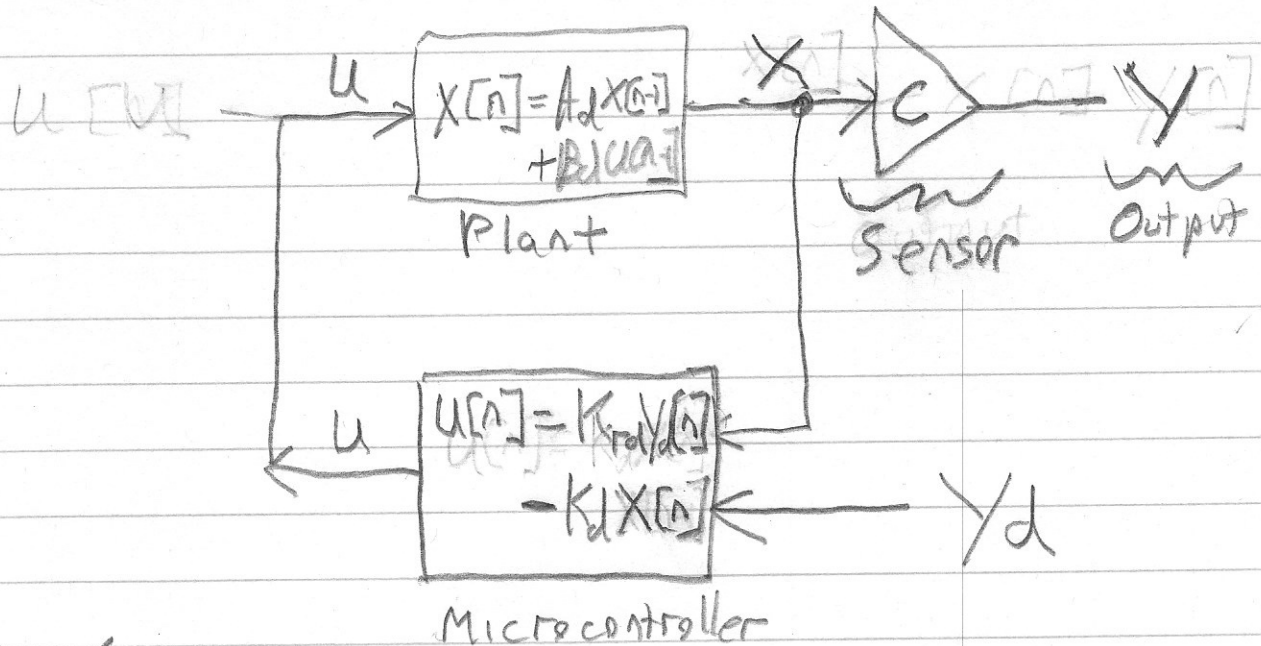
or if  $Q$  &  $R$  diagonal

$$\sum_{m=0}^{\infty} \left( \sum_{i=1}^{\# \text{ states}} Q_{ii} X_i^2[m] \right) + \left( \sum_{j=1}^{\# \text{ inputs}} R_{jj} u_j^2[m] \right)$$

4A

What about  $K_d$ ?

Plant Model  $\left\{ \begin{array}{l} x[n] = A_d x[n-1] + B_d u[n-1] \\ y[n] = C x[n] \end{array} \right.$



Controller  $\left\{ \begin{array}{l} u[n] = K_d y_d[n] - K_d x[n] \end{array} \right.$

$\uparrow$  ?  
 $\uparrow$  minimize metric

Closed-Loop

$$x[n] = (A_d - B_d K_d) x[n-1] + B_d K_d y_d[n-1]$$

In Steady State  $x[n] \rightarrow x_{\infty}$   $y_d[n] \rightarrow y_{\infty}$

$$x_{\infty} = (A_d - B_d K_d) x_{\infty} + B_d K_d y_{\infty}$$



What is Krd (Continued)

(4B)

In Steady State (Continued)

$$(I - (A_d - B_d K_d)) X_\infty = B_d K_d Y_{d_\infty}$$

$$\Rightarrow \underbrace{X_\infty}_{\substack{\text{Vector} \\ n \times 1}} = \underbrace{(I - (A_d - B_d K_d))^{-1}}_{\substack{\text{matrix} \\ n \times n}} \underbrace{B_d K_d}_{\substack{\text{Vector} \\ 1 \times 1}} \underbrace{Y_{d_\infty}}_{\substack{\text{Scalar} \\ 1 \times 1}}$$

$$\underbrace{Y_\infty}_{\substack{\uparrow \\ \text{scalar}}} = C X_\infty = C \underbrace{(I - (A_d - B_d K_d))^{-1}}_{\substack{\uparrow \\ \text{matrix} \\ n \times n}} \underbrace{B_d K_d}_{\substack{\uparrow \\ \text{Vector} \\ 1 \times 1}} \underbrace{Y_{d_\infty}}_{\substack{\uparrow \\ \text{Scalar} \\ 1 \times 1}}$$

should match in steady-state

$$\frac{Y_\infty}{Y_{d_\infty}} = 1 = \underbrace{C (I - (A_d - B_d K_d))^{-1} B_d}_{\substack{\text{Scalar}}} \underbrace{K_d}_{\substack{\uparrow \\ \text{Scalar}}}$$

---

$$\frac{1}{C (I - (A_d - B_d K_d))^{-1} B_d} = K_d !!$$

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# Discrete-Time Observers

$u$

$$\hat{x}[n] = A_d \hat{x}[n-1] + \underbrace{B_d u[n-1]}_{\text{No hat, we know } u}$$

No hat, we know u

$$+ \underbrace{L_d (y[n-1] - \hat{y}[n-1])}_{\text{correction}}$$

$$u[n-1] = K_d y[n-1] - K_d \hat{x}[n-1]$$

Compare  
Indexing

On a microcontroller

→ Every  $\Delta T$  interval

1) Using predicted state, create control

$$u \leftarrow K_d y - K_d \hat{x}$$

2) Measure observable and compare

$$\text{correction} \leftarrow L_d (y - \hat{y})$$

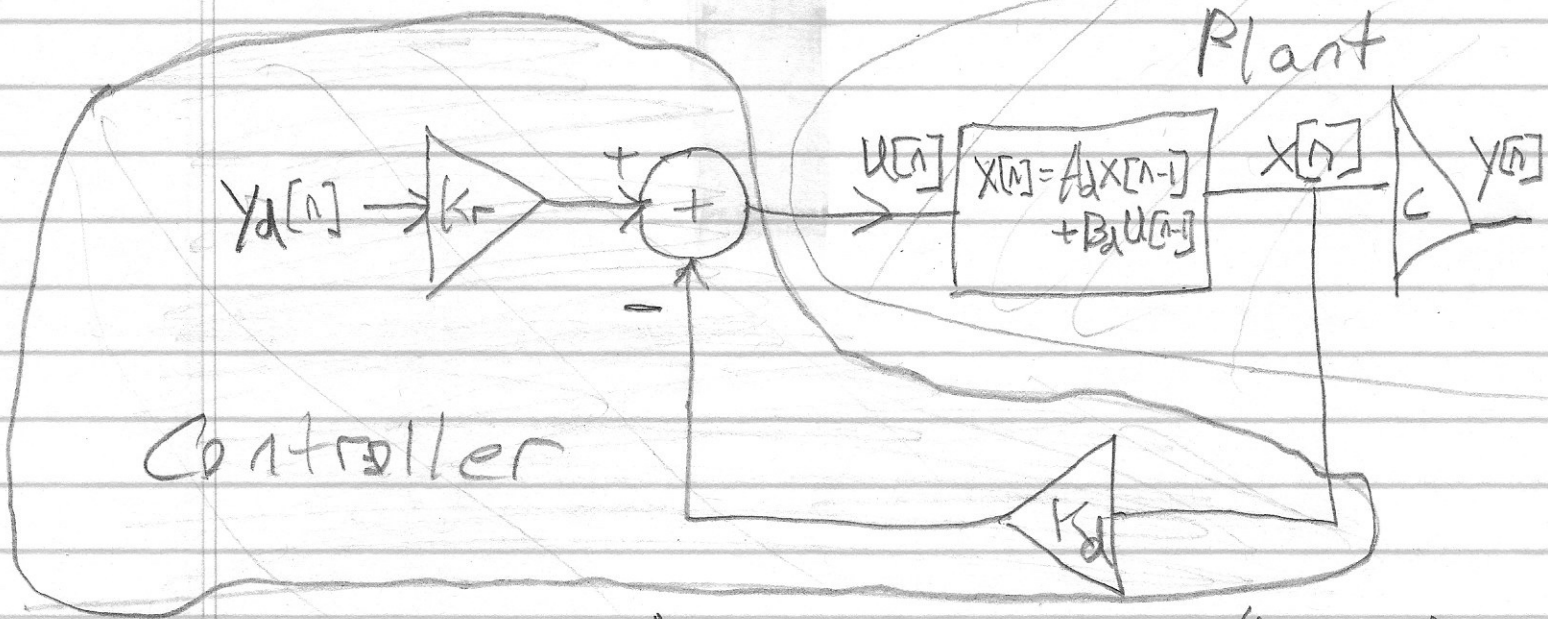
3) Update estimates of state & observable

$$\hat{x} \leftarrow A_d \hat{x} + B_d u + \text{correction}$$

$$\hat{y} \leftarrow C \hat{x}$$

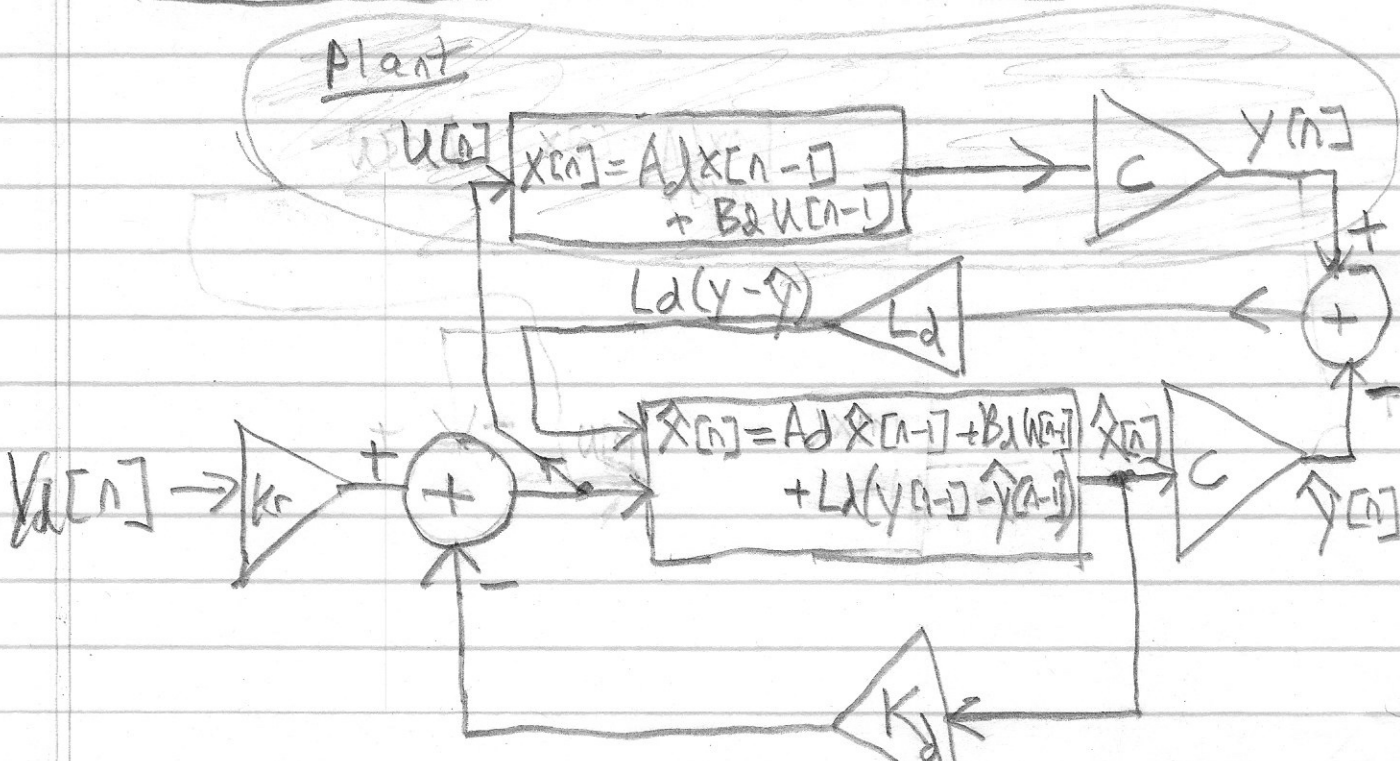
5A

Measured-State Feedback



$$x[n] = A_d x[n-1] + B_d u[n] = (A_d - B_d K_d) x[n-1] + B_d K_r y_d[n]$$

Observer - State Feedback



$$x[n] = A_d x[n-1] - B_d K_d \hat{x}[n-1] + B_d K_r r[n]$$

$$\hat{x}[n] = A (A_d - B_d K_d - L_d C) \hat{x}[n-1] + L_d C x[n-1] + B_d K_r y[n]$$

# Analyze Coupled System

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Actual:  $x[n] = A_d x[n-1] + B_d u[n-1]$

Estimate:  $\hat{x}[n] = A_d \hat{x}[n-1] + B_d u[n-1] + L_d (y[n-1] - \hat{y}[n-1])$

$$e_{rr}[n] \equiv x[n] - \hat{x}[n]$$

$$\Rightarrow \hat{x}[n] = x[n] - e_{rr}[n]$$

Subtracting

$$\underbrace{x[n] - \hat{x}[n]}_{e_{rr}[n]} = A_d \left( \underbrace{x[n-1] - \hat{x}[n-1]}_{e_{rr}[n-1]} \right) - L_d \underbrace{(y[n-1] - \hat{y}[n-1])}_{C e_{rr}[n-1]}$$

$$e_{rr}[n] = A_d e_{rr}[n-1] - L_d C_d e_{rr}[n-1] \\ = (A_d - L_d C_d) e_{rr}[n-1]$$

$e_{rr}$  does not depend on  $K_d$ !

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# Coupled System Continued

## Closed-Loop Control using Observer

$$x[n] = A_d x[n-1] + B_d (K_d x[n-1] - K_d \hat{x}[n-1])$$

Since  $\hat{x}[n-1] = x[n-1] - e[n-1]$

$$\Rightarrow x[n] = (A_d - B_d K_d) x[n-1]$$

$$e[n] = \hat{x}[n] - x[n] + B_d K_d e[n-1] + B_d K_d y_d[n-1]$$

### Compare to Closed loop measured-state

Assuming  $x_r[n] = (A_d - B_d K_d) x_r[n-1] + B_d K_d y_d[n-1]$

$u = K_d y_d - K_d x$   
measured state

$x_r$  is state if measured state feedback is used

$$(x[n] - x_r[n]) = (A_d - B_d K_d)(x[n-1] - x_r[n-1]) + B_d K_d e[n-1]$$

State using observed state feedback

state using measured state feedback

Observer Feedback like "Real" State Feedback if  $e \rightarrow 0$  fast

## Relation between $K_d$ & $L_d$

8

If eig  $(A_d - L_d C_d)$  are smaller than the eig  $(A_d - B_d K_d)$

Then State-Feedback with estimated state will perform like state-feedback with measured state.

Why not pick  $L_d$  such that

$$\max_i |\lambda_i(A_d - L_d C_d)| \approx 0!$$

Because large values of  $L_d$  are bad!

# Noise Example with Measurement Noise

With noise

$$e_{rr}[n] = A_d e_{rr}[n-1]$$

$$- L_d (y[n-1] - \hat{y}[n-1] + W[n])$$

Suppose  $W[n] = W_0$  (constant noise)

Noise

$$e_{rr}[n] = (A_d - L_d C_d) e_{rr}[n-1] + L_d W_0$$

In steady-state  $e_{rr}[n] = e_{rr}[n-1] = e_{rr}[\infty]$

$$(I - (A_d - L_d C_d)) e_{rr}[\infty] = L_d W_0$$

$$e_{rr}[\infty] = (I - (A_d - L_d C_d))^{-1} L_d W_0$$

Best Case! IF  $L_d$ 's chosen for very fast decay

$$A_d - L_d C_d \approx 0 \Rightarrow (I - (A_d - L_d C_d))^{-1} \approx I$$

and  $e_{rr}[\infty] \approx L_d W_0$  Big Ld Big Errors

Even if Best case

Large  $L_d$ 's

mean high sensitivity to measurement

Noise!