6.3100: Dynamic System Modeling and Control Design

CT Frequency Response

merge with CT_Frequency_Response_2

October 16, 2024

Retrospective: Eigenfunctions and Eigenvalues

If a system contains only adders, gains, differentiators, and integrators, then its system function can be written as a rational polynomial in *s*:

$$
H(s)=\frac{Y}{X}
$$

The eigenfunctions of such systems are **complex exponentials** $(e^{s_0 t})$ and associated eigenvalues are given by the system function evaluated at *s*0.

Retrospective: Frequency Response

The response of such a system to a sinusoidal input is determined by its system function $H(s)$ evaluated at $s = j\omega_0$.

$$
e^{j\omega_0 t} \to H(j\omega_0)e^{j\omega_0 t}
$$

\n
$$
e^{-j\omega_0 t} \to H(-j\omega_0)e^{-j\omega_0 t}
$$

\n
$$
\cos(\omega_0 t) = \frac{1}{2} \Big(e^{j\omega_0 t} + e^{-j\omega_0 t} \Big) \to \frac{1}{2} \Big(H(j\omega_0)e^{j\omega_0 t} + H(-j\omega_0)e^{-j\omega_0 t} \Big)
$$

\n
$$
\to \text{Re} \left(H(j\omega_0)e^{j\omega_0 t} \right)
$$

\n
$$
\to \text{Re} \left(|H(j\omega_0)|e^{j\angle H(j\omega_0)}e^{j\omega_0 t} \right)
$$

\n
$$
\to |H(j\omega_0)| \text{ Re } \left(e^{j\angle H(j\omega_0) + j\omega_0 t} \right)
$$

\n
$$
\to |H(j\omega_0)| \cos(\omega_0 t + \angle H(j\omega_0))
$$

$$
\cos(\omega_0 t) \longrightarrow H(s) \Big|_{s=j\omega_0} \longrightarrow |H(j\omega_0)| \cos(\omega_0 t + \angle H(j\omega_0))
$$

Retrospective: Poles and Zeros

If a system contains only adders, gains, differentiators, and integrators, then its system function can be written as a rational polynomial in *s*:

$$
H(s) = \frac{b_0 + b_1s + b_2s^2 + b_3s^3 + \cdots}{a_0 + a_1s + a_2s^2 + a_3s^3 + \cdots}
$$

The numerator and denominator polynomials can be factored into products of terms: one for each zero in the numerator or pole in the denominator:

$$
H(s) = K \frac{(s - z_0)(s - z_1)(s - z_2) \cdots}{(s - p_0)(s - p_1)(s - p_2) \cdots}
$$

Even a complicated system is completely described by a small number of constants: K , z_0 , p_0 , z_1 , p_1 , z_2 , p_2 ,...

Vector Interpretation of the Frequency Response

The frequency response of a system is determined by the ratio of the product of vectors from each zero to the point $j\omega_0$ divided by the product of vectors from each pole to the point $j\omega_0$.

$$
H(j\omega_0) = K \frac{(j\omega_0 - z_0)(j\omega_0 - z_1)(j\omega_0 - z_2)\cdots}{(j\omega_0 - p_0)(j\omega_0 - p_1)(j\omega_0 - p_2)\cdots}
$$

While this approach is simple (compared to solving a differential equation), using **Bode Diagrams** is even simpler.

Frequency Response: Single Zero

Asymptotic Behavior: Single Zero

The magnitude response is simple at low and high frequencies.

Asymptotic Behavior: Single Zero

Two asymptotes provide a good approximation on log-log axes.

 $\lim_{\omega \to 0} |H(j\omega)| = |z_1|$ $\lim_{\omega \to \infty} |H(j\omega)| = \omega$

Frequency Response: Single Pole

Frequency Response: Single Pole

Frequency Response: Single Pole

Asymptotic Behavior: Single Pole

The magnitude response is simple at low and high frequencies.

Asymptotic Behavior: Single Pole

Two asymptotes provide a good approximation on log-log axes.

Compare log-log plots of the frequency-response magnitudes of the following system functions:

$$
H_1(s) = \frac{1}{s+1}
$$
 and $H_2(s) = \frac{1}{s+10}$

The former can be transformed into the latter by

- 1. shifting horizontally
- 2. shifting and scaling horizontally
- 3. shifting both horizontally and vertically
- 4. shifting and scaling both horizontally and vertically
- 5. none of the above

Asymptotic Behavior of More Complicated Systems

Constructing $H(s_0)$.

$$
H(s_0) = K \frac{\prod_{q=1}^{Q} (s_0 - z_q)}{\prod_{p=1}^{P} (s_0 - p_p)} \leftarrow \text{product of vectors for zeros}
$$

Asymptotic Behavior of More Complicated Systems

The magnitude of a product is the product of the magnitudes.

$$
|H(s_0)| = \left| K \frac{\prod_{q=1}^{Q} (s_0 - z_q)}{\prod_{p=1}^{P} (s_0 - p_p)} \right| = |K| \frac{\prod_{q=1}^{Q} |s_0 - z_q|}{\prod_{p=1}^{P} |s_0 - p_p|}
$$

The log of the magnitude is a sum of logs.

$$
|H(s_0)| = \left| K \frac{\prod_{q=1}^{Q} (s_0 - z_q)}{\prod_{p=1}^{P} (s_0 - p_p)} \right| = |K| \frac{\prod_{q=1}^{Q} |s_0 - z_q|}{\prod_{p=1}^{P} |s_0 - p_p|}
$$

$$
\log |H(j\omega)| = \log |K| + \sum_{q=1}^{Q} \log |j\omega - z_q| - \sum_{p=1}^{P} \log |j\omega - p_p|
$$

Bode Plot: Adding Instead of Multiplying

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Asymptotic Behavior: Single Zero

The angle response is simple at low and high frequencies.

Asymptotic Behavior: Single Zero

Three straight lines provide a good approximation versus log *ω*.

Asymptotic Behavior: Single Pole

The angle response is simple at low and high frequencies.

Asymptotic Behavior: Single Pole

Three straight lines provide a good approximation versus log *ω*.

The angle of a product is the sum of the angles.

$$
\angle H(s_0) = \angle \left(K \frac{\prod_{q=1}^{Q} (s_0 - z_q)}{\prod_{p=1}^{P} (s_0 - p_p)} \right) = \angle K + \sum_{q=1}^{Q} \angle (s_0 - z_q) - \sum_{p=1}^{P} \angle (s_0 - p_p)
$$

The angle of K can be 0 or π .

From Frequency Response to Bode Plot

The magnitude of $H(j\omega)$ is a product of magnitudes.

$$
|H(j\omega)| = |K| \frac{\prod_{q=1}^{Q} |j\omega - z_q|}{\prod_{p=1}^{P} |j\omega - p_p|}
$$

The log of the magnitude is a sum of logs.

$$
\log |H(j\omega)| = \log |K| + \sum_{q=1}^{Q} \log |j\omega - z_q| - \sum_{p=1}^{P} \log |j\omega - p_p|
$$

The angle of $H(j\omega)$ is a sum of angles.

$$
\angle H(j\omega) = \angle K + \sum_{q=1}^{Q} \angle (j\omega - z_q) - \sum_{p=1}^{P} \angle (j\omega - p_p)
$$

5. none of the above

Bode Plot: dB

Bode Plot: dB

Bode Plot: Accuracy

The straight-line approximations are surprisingly accurate.

Complex-Valued Poles and Zeros

New issues arise for complex-valued poles and zeros.

We have previously seen that complex-valued poles are associated with resonance. How does resonance affect a Bode plot?

The frequency-response magnitude of a high-Q system is peaked.

 $Q = 0.501$

The frequency-response magnitude of a high-Q system is peaked.

 $Q = 1$ *s ω*0 plane −1 − 1 2*Q* ¹ 1 − $\sqrt{1}$ 2*Q* \setminus^2 − ¹ 1 − $\sqrt{ }$ 1 2*Q* $\frac{1}{2}$ ⁻² $H(s) = \frac{1}{s}$ $1 + \frac{1}{6}$ *Q s* $\frac{s}{\omega_0}+\bigg(\frac{s}{\omega_0}$ *ω*0 \setminus^2 -2 -1 0 1 2 0 −1 $\log \frac{\omega}{\omega}$ *ω*0 $\log|H(j\omega)|$

−

1 −

The frequency-response magnitude of a high-Q system is peaked.

 $Q = 16$ *s ω*0 plane −1 − 1 2*Q* ¹ 1 − $\sqrt{1}$ 2*Q* \setminus^2 ¹ $\frac{1}{2}$ $\frac{1}{2Q}$ ² $H(s) = \frac{1}{s}$ $1 + \frac{1}{6}$ *Q s* $\frac{s}{\omega_0}+\bigg(\frac{s}{\omega_0}$ *ω*0 \setminus^2 0 −1 −2 $\log \frac{\omega}{\omega}$ $\log|H(j\omega)|$

 -2 -1 0 1 2

*ω*0

As *Q* increases, the phase changes more abruptly with *ω*.

 $Q = 0.501$

$$
H(s) = \frac{1}{1 + \frac{1}{Q}\frac{s}{\omega_0} + \left(\frac{s}{\omega_0}\right)^2}
$$
\n
$$
\frac{s}{\omega_0} \text{ plane}
$$
\n
$$
0
$$
\n
$$
-\pi/2
$$
\n
$$
-\pi
$$
\n
$$
-\pi
$$
\n
$$
-2
$$
\n
$$
-1
$$
\n
$$
0
$$
\n
$$
-\pi/2
$$
\n
$$
-2
$$
\n
$$
10g\frac{\omega}{\omega_0}
$$

As *Q* increases, the phase changes more abruptly with *ω*.

$$
Q=8
$$

$$
H(s) = \frac{1}{1 + \frac{1}{Q} \frac{s}{\omega_0} + \left(\frac{s}{\omega_0}\right)^2}
$$

Consider the system represented by the following poles. *ω*0 −*ω*⁰ *s*-plane −*σ ωd* −*ω^d* Find the frequency ω_r at which the magnitude of the response *y*(*t*) is greatest if $x(t) = \cos \omega_r t$. 1. $\omega_r > \omega_0$ 2. $\omega_r = \omega_0$

3. $\omega_d < \omega_r < \omega_0$ 4. $\omega_r = \omega_d$

5. $\omega_r < \omega_d$

5. $\omega < \omega_d$

Summary

The frequency response of a system is easily determined using Bode plots.

Each pole and each zero contributes one section to the Bode plot.

The magnitude of the response of the system is given by the sum of the log magnitudes for the sections contributed by each pole and zero.

The angle of the response of the system is given by the sum of the angles for the sections contributed by each pole and zero.