6.3100: Dynamic System Modeling and Control Design

Observer Design

November 25, 2024

Last time, we introduced the notion of an observer, which is a model of a plant that is used to improve performance of a controller.



We embed both the plant and observer in state-space controllers, so that the simulation can provide estimates of the state  $(\hat{\mathbf{x}}(t))$  and input  $(\hat{u}(t))$ .



If feedback from all of the states in  $x(t)$  is not possible ...



we can substitute the simulated states  $\hat{\mathbf{x}}(t)$  for the missing states  $\mathbf{x}(t)$ . Similarly, we can substitute  $\hat{u}(t)$  for  $u(t)$  as well.



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Unfortunately the resulting system is feedforward. It's utility depends critically on the accuracy of the match between the plant and observer.



Fortunately, we can use feedback to measure and correct simulation errors! Calculate the difference between  $y(t)$  and  $\hat{y}(t)$ . Then use that signal (times **L**) to correct  $\hat{\mathbf{x}}(t)$ .



Analyze by finding matrix expressions for the derivatives of the states. Plant dynamics:  $\dot{\mathbf{x}}(t) = \mathbf{A}\mathbf{x}(t) - \mathbf{B}\mathbf{K}\hat{\mathbf{x}}(t) + \mathbf{B}K_r y_d(t)$ Simulation dynamics:  $\hat{\mathbf{x}}(t) = \mathbf{A}\hat{\mathbf{x}}(t) - \mathbf{B}\mathbf{K}\hat{\mathbf{x}}(t) + \mathbf{B}K_r y_d(t) + \mathbf{L}(y(t)-\hat{y}(t))$ 



Combined dynamics of the plant and observer.

$$
\dot{\mathbf{x}}(t) = \mathbf{A}\mathbf{x}(t) - \mathbf{B}\mathbf{K}\hat{\mathbf{x}}(t) + \mathbf{B}K_r y_d(t)
$$

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\dot{\mathbf{x}}(t) = \mathbf{A}\hat{\mathbf{x}}(t) - \mathbf{B}\mathbf{K}\hat{\mathbf{x}}(t) + \mathbf{B}K_r y_d(t) + \mathbf{L}(y(t) - \hat{y}(t))
$$

Define  $e(t)$  to be the difference between the plant and simulation states:

$$
\mathbf{e}(t) = \mathbf{x}(t) - \hat{\mathbf{x}}(t)
$$

Subtract  $\dot{\hat{\mathbf{x}}}(t)$  from  $\dot{\mathbf{x}}(t)$  to find the derivative of  $\mathbf{e}(t)$ :

$$
\dot{\mathbf{e}}(t) = \mathbf{A}\mathbf{e}(t) - \mathbf{L}\Big(y(t) - \widehat{y}(t)\Big) = \mathbf{A}\mathbf{e}(t) - \mathbf{L}\mathbf{C}\mathbf{e}(t)
$$

Append the  $\dot{\mathbf{x}}(t)$  and  $\dot{\mathbf{e}}(t)$  to make a new **combined** state vector:

$$
\begin{bmatrix} \dot{\mathbf{x}}(t) \\ \dot{\mathbf{e}}(t) \end{bmatrix} = \begin{bmatrix} \mathbf{A} - \mathbf{B} \mathbf{K} & \mathbf{B} \mathbf{K} \\ \mathbf{0} & \mathbf{A} - \mathbf{L} \mathbf{C} \end{bmatrix} \begin{bmatrix} \mathbf{x}(t) \\ \mathbf{e}(t) \end{bmatrix} + \begin{bmatrix} \mathbf{B} \\ \mathbf{0} \end{bmatrix} K_r y_d(t)
$$

Combined dynamics of the plant and observer.

$$
\begin{bmatrix} \dot{\mathbf{x}}(t) \\ \dot{\mathbf{e}}(t) \end{bmatrix} = \begin{bmatrix} \mathbf{A} - \mathbf{B} \mathbf{K} & \mathbf{B} \mathbf{K} \\ \mathbf{0} & \mathbf{A} - \mathbf{L} \mathbf{C} \end{bmatrix} \begin{bmatrix} \mathbf{x}(t) \\ \mathbf{e}(t) \end{bmatrix} + \begin{bmatrix} \mathbf{B} \\ \mathbf{0} \end{bmatrix} K_r y_d(t)
$$

The poles of this system are the roots of its characteristic equation:

$$
\left| s\mathbf{I} - \begin{bmatrix} \mathbf{A} - \mathbf{B} \mathbf{K} & \mathbf{B} \mathbf{K} \\ \mathbf{0} & \mathbf{A} - \mathbf{L} \mathbf{C} \end{bmatrix} \right| = 0
$$

Because the evolution matrix has block triangular form, the characteristic equation can be factored into two parts:

$$
\left| s\mathbf{I} - \begin{bmatrix} \mathbf{A} - \mathbf{B} \mathbf{K} & \mathbf{B} \mathbf{K} \\ \mathbf{0} & \mathbf{A} - \mathbf{L} \mathbf{C} \end{bmatrix} \right| = \left| s\mathbf{I} - (\mathbf{A} - \mathbf{B} \mathbf{K}) \right| \times \left| s\mathbf{I} - (\mathbf{A} - \mathbf{L} \mathbf{C}) \right| = 0
$$

and the poles of the augmented system are the union of the poles of the plant and simulation dynamics.

Furthermore, K can be chosen to optimize  $A-BK$  and **L** can be chosen to optimize  $A-LC$ .

We've seen the first part of this problem before!

# Linear Quadratic Regulator (LQR) – Redux!

The LQR method minimizes a cost function *J* that weighs the squares of the state variables  $\mathbf{x}(t)$  and input  $\mathbf{u}(t)$ .

$$
J = \int_0^\infty \left( \mathbf{x}^{\mathbf{T}}(t) \, \mathbf{Q} \mathbf{x}(t) + \mathbf{u}^{\mathbf{T}}(t) \, \mathbf{R} \mathbf{u}(t) \right) dt
$$

where  $\mathbf{u}(t)$  and  $\mathbf{x}(t)$  are related

- by the state transition equation:  $\dot{\mathbf{x}}(t) = \mathbf{A}\mathbf{x}(t) + \mathbf{B}\mathbf{u}(t)$  and
- by the feedback constraint:  $\mathbf{u}(t) = -\mathbf{K}\mathbf{x}(t)$ .

and  $Q$  and  $R$  represent weights.

The "optimal"  $\bf{K}$  is given by

 $K = \mathbf{R}^{-1} \mathbf{B}^{\mathbf{T}} \mathbf{S}$ 

where S is the symmetric  $n \times n$  solution to the **algebraic Riccati equation**:

 $\mathbf{A^T S} + \mathbf{S A} - \mathbf{S B R^{-1} B^T S} + \mathbf{Q} = \mathbf{0}$ 

## Linear Quadratic Regulator (LQR) – Double Redux!

The LQR method minimizes a **cost function** J' that weighs the squares of observer state errors  $\hat{\mathbf{e}}(t) = \mathbf{x}(t) - \hat{\mathbf{x}}(t)$  and observer output errors  $y(t) - \hat{y}(t)$ .

$$
J' = \int_0^\infty \left( \mathbf{e}(t)^T \mathbf{Q} \mathbf{e}(t) + (y(t) - \widehat{y}(t))^T \mathbf{R} (y(t) - \widehat{y}(t) \right) dt
$$

where  $(y(t)-\widehat{y}(t))$  and  $e(t)$  are related

- by a state transition equation:  $\dot{\mathbf{e}}(t) = \mathbf{A}\mathbf{e}(t) \mathbf{L}(y(t) \hat{y}(t))$  and<br>• by the feedback constraint:  $y(t) \hat{y}(t) = \mathbf{C}\mathbf{e}(t)$
- by the feedback constraint:  $y(t)-\hat{y}(t) = \mathbf{C}\mathbf{e}(t)$ .

and  $Q$  and  $R$  represent weights.

The "optimal"  $L$  is given by

 $\mathbf{L}^{\mathbf{T}} = \mathbf{R}^{-1}\mathbf{C}\mathbf{S}$ 

*J*

where S is the symmetric  $n \times n$  solution to the **algebraic Riccati equation**:

 $\mathbf{AS} + \mathbf{SA^T} - \mathbf{SC^TR^{-1}CS} + \mathbf{Q} = \mathbf{0}$ 

# Choosing K and L

Since optimizing  $K$  and  $L$  can be cast into problems with the same form, the optimizations can be solved using the same methods.

```
K = place(A, B, [poles])
```

```
L = transpose(place(transpose(A), transpose(C), [poles]))
```
or

 $K = \text{lgr}(A, B, Qk, Rk)$ 

```
L = \text{transpose}(\text{lgr}(\text{transpose}(A), \text{transpose}(C), Q1, R1))
```
#### Example: propeller arm (lab 6)





Substitute  $A$ ,  $B$ , and  $C$  into the observer framework.

Plant dynamics:  $\dot{\mathbf{x}}(t) = \mathbf{A}\mathbf{x}(t) - \mathbf{B}\mathbf{K}\hat{\mathbf{x}}(t) + \mathbf{B}K_r y_d(t)$ Simulation dynamics:  $\dot{\hat{\mathbf{x}}}(t) = \mathbf{A}\hat{\mathbf{x}}(t) - \mathbf{B}\mathbf{K}\hat{\mathbf{x}}(t) + \mathbf{B}K_r y_d(t) + \mathbf{L}(y(t)-\hat{y}(t))$ 



Effect of increasing *Qk*'s.



Responses of plant and observer match. Why? Responses for different *Qk*'s match. Why?

Plant and observer responses match because model parameters match.



Responses for different Qk's matched because *u*(*t*) was very small. Need much bigger Rk (shown here) for Qk to be important.

Effect of increasing  $Q_k[0], Q_k[1]$ , and  $Q_k[2]$  – one at a time.



Which column shows

Qk:100,1,1? Qk:1,100,1? Qk:1,1,100?

Effect of increasing  $Q_k[0], Q_k[1]$ , and  $Q_k[2]$  – one at a time.



Which column shows

Qk:100,1,1? middle; Qk:1,100,1? left; Qk:1,1,100? right

Effect of increasing *Q<sup>l</sup>* 's.



Responses of plant and observer match. Why? Responses for different  $Q_l$ 's match. Why?

### Observer Mismatch

What if the observer does not match the plant? What if the red  $\bf{B}$  is different from the green  $\bf{B}$ ?



Effect of increasing  $Q_k$ 's when  $\gamma_a$  for plant is half that for observer.



Increasing **K**'s by increasing  $Q_k$ 's has little effect on mismatch. Why?

Effect of increasing  $Q_l$ 's when  $\gamma_a$  for plant is half that for observer.



Increasing  ${\bf L}$ 's by increasing  $Q_l$ 's improves match (especially for  $\theta(t)).$ 

Effect of increasing  $Q_l$ 's one at a time.



Better to assess  $L$  using differences between plant and observer variables.

To choose  $K$ , we minimize a cost function  $J$  that weighs the squares of the state variables  $\mathbf{x}(t)$  and input  $\mathbf{u}(t)$ :

$$
J = \int_0^\infty \left( \mathbf{x}^{\mathbf{T}}(t) \, \mathbf{Q} \mathbf{x}(t) + \mathbf{u}^{\mathbf{T}}(t) \, \mathbf{R} \mathbf{u}(t) \right) dt
$$

The most effective **K** is the one that minimizes the squared values of  $\mathbf{x}(t)$ and  $\mathbf{u}(t)$ .

To choose L, we minimize a cost function  $J'$  that weighs the squares of observer state errors  $\mathbf{e}(t) = \mathbf{x}(t) - \hat{\mathbf{x}}(t)$  and observer output errors  $y(t) - \hat{y}(t)$ :

$$
J' = \int_0^\infty \left( \mathbf{e}(t)^T \mathbf{Q} \mathbf{e}(t) + (y(t) - \widehat{y}(t))^T \mathbf{R} (y(t) - \widehat{y}(t) \right) dt
$$

The most effective **L** is the one that minimizes the squared values of  $e(t)$ and  $y(t) - \widehat{y}(t)$ .

Effect of increasing  $Q_l$ 's one at a time.



Which column shows

Ql:100,0,0? Ql:0,100,0? Ql:0,0,100?

Effect of increasing  $Q_l$ 's one at a time.



Which column shows

Ql:100,0,0? left; Ql:0,100,0? middle; Ql:0,0,100? little difference

### Next Time

No lecture on Wednesday. No office hours on Wednesday. Happy Thanksgiving!