Dynamic System Modeling and Control Design Second Order DT System, Proportional and PD Control

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#### 2 Proportional Controller Shortcomings



**3** New Controller: Proportional Derivative

# Line Following Example

Consider a line following example illustrated below:



$$d[n] = d[n-1] + \Delta TV \sin \theta[n-1],$$
  

$$\theta[n] = \theta[n-1] + \Delta T\omega[n-1],$$
  

$$\omega[n] = \gamma u[n].$$

Goal: control the angular velocity of the robot to follow the line.

• Assume we have an optical sensor to measure the distance,  $d_m$ .

## Small Adjustments...

Assume that we are operating in a small  $\theta$  regime such that  $\sin \theta \approx \theta$ .



Goal: control the angular velocity of the robot to follow the line.

• Assume we have an optical sensor to measure the distance,  $d_m$ .

### Towards a System Equation

Now, we need a system equation with respect to the measured distance. Consider the difference between  $d_m[n]$  and  $d_m[n-1]$ :

$$d_m[n] = d_m[n-1] + \Delta T V \theta[n-1] - d_m[n-1] = d_m[n-2] + \Delta T V \theta[n-2] d_m[n] - d_m[n-1] = d_m[n-1] - d_m[n-2] + \Delta T V (\theta[n-1] - \theta[n-2])$$

With some rearranging:

$$d_m[n] - 2d_m[n-1] + d_m[n-2] = \Delta TV \left(\theta[n-1] - \theta[n-2]\right)$$

# Line Following System Equation

Recall that we have:

$$\theta[n] = \theta[n-1] + \Delta T \omega[n-1] = \theta[n-1] + \Delta T \gamma u[n-1].$$

Therefore,  $\theta[n] - \theta[n-1] = \Delta T \gamma u[n-1]$ , and we obtain:

$$d_m[n] - 2d_m[n-1] + d_m[n-2] = \Delta TV \left(\theta[n-1] - \theta[n-2]\right)$$

$$\Rightarrow d_m[n] - 2d_m[n-1] + d_m[n-2] = \Delta T^2 V \gamma u[n-2]$$

Now, we need to pick our control signal, u[n].

# How About Proportional Control?

First, let's attempt to use proportional control,

$$u[n] = K_p(d_d[n] - d_m[n]).$$

$$d_m[n] - 2d_m[n-1] + d_m[n-2] =$$
  

$$\Delta T^2 V \gamma K_p(d_d[n-2] - d_m[n-2])$$
  

$$\Rightarrow d_m[n] - 2d_m[n-1] + (1 + \Delta T^2 V K_p \gamma) d_m[n-2] =$$
  

$$\Delta T^2 V \gamma K_p d_d[n-2]$$

Now, we have a second order difference equation for  $d_m[n]$ .

# Check Yourself: Step Response

Modify the code from last lecture (link) to plot the step response of this second order system:

$$d_m[n] - 2d_m[n-1] + (1 + \Delta T^2 V K_p \gamma) d_m[n-2] = \Delta T^2 V \gamma K_p d_d[n-2],$$

with the following parameters:

- $K_p = 5$ ,
- $\gamma = 1$ ,
- V = 1,
- $\Delta T = 0.01$ ,
- simulation\_time = 25,

by defining a new transfer function. Be prepared to show the plot!

#### Homogeneous Solution of Second Order DT System

For a second order DT system, the general solution is given by:

$$d_m[n] = C_1 \lambda_1^n + C_2 \lambda_2^n,$$

where  $\lambda_1, \lambda_2$  are natural frequencies,  $C_1, C_2$  are coefficients determined by the initial conditions.

The homogeneous solution is given by:

$$\lambda^{n} - 2\lambda^{n-1} + (1 + \Delta T^{2}VK_{p}\gamma)\lambda^{n-2} = 0$$
$$\lambda^{2} - 2\lambda + (1 + \Delta T^{2}VK_{p}\gamma) = 0$$
$$\Rightarrow \boxed{\lambda = 1 \pm j\sqrt{\Delta T^{2}VK_{p}\gamma}}$$

## A Complex Result...

The natural frequencies for the proportional controller are,

$$\lambda = 1 \pm j \sqrt{\Delta T^2 V K_p \gamma}.$$

- $\lambda_1, \lambda_2$  will be complex numbers
- ...with magnitude strictly great than 1!
- This system is always unstable regardless of  $K_p$ .

### Root Locus Plot



$$\lambda = 1 \pm j \sqrt{\Delta T^2 V K_p \gamma}.$$

- When  $K_p = 0, \lambda = 1$ .
- As  $K_p \to \infty$ , moves vertically away from real axis.

# Proportional-Derivative (PD) Controller

New controller: the proportional-derivative (PD) controller:

$$u[n] = K_p \left( d_d[n] - d_m[n] \right) + K_d \left( \frac{d_d[n] - d_d[n-1]}{\Delta T} - \frac{d_m[n] - d_m[n-1]}{\Delta T} \right)$$

This controller not only cares about the relative distance, but also the rate of change.

### System Equation with Proportional Derivative Control

From the original system equation,

$$d_m[n] - 2d_m[n-1] + d_m[n-2] = \Delta T^2 V \gamma u[n-2],$$

we can plug in our new PD controller:

$$\begin{aligned} d_m[n] - 2d_m[n-1] + d_m[n-2] &= \\ \Delta T^2 V \gamma \left[ K_p \left( d_d[n-2] - d_m[n-3] \right) + K_d \left( \frac{d_d[n-2] - d_d[n-3]}{\Delta T} - \frac{d_m[n-2] - d_m[n-3]}{\Delta T} \right) \right] \end{aligned}$$

We will skip the algebra necessary to rearrange this equation...

## Third Order Characteristic Equation

We obtain the following characteristic equation:

$$d_m[n] - 2d_m[n-1] + (1 + \Delta T^2 V \gamma K_p + K_d V \gamma \Delta T) d_m[n-2] - K_d V \gamma \Delta T d_m[n-3]$$
  
=  $(\Delta T^2 \gamma V K_p + K_d \Delta T V \gamma) d_d[n-2] - K_d \Delta T V \gamma d_d[n-3]$ 

This is a third order difference equation, which has the following solution:

$$d_m[n] = C_1 \lambda_1^n + C_2 \lambda_2^n + C_3 \lambda_3^n.$$

Now there are 3 natural frequencies! Each are a function of  $K_p$  and  $K_d$ .

# Third Order System in Python

```
# Define the system parameters
Kp = 5
Kd = 1
gamma = 1
V = 1
dt = 0.01
```

```
# Define the transfer function
num = np.array([0, 0, dt**2*V*gamma*Kp+Kd*V*gamma*dt, -Kd*V*gamma*dt])
den = np.array([1, -2, 1+dt**2*V*gamma*Kp+Kd*V*gamma*dt, -Kd*V*gamma*dt])
```

```
# Define our third-order system
system = ctrl.TransferFunction(num,den,dt=dt)
```

```
# Get step response
time = np.arange(0, 25, dt) # Create the time vector
_, response = ctrl.step_response(system, T=time)
```

### Third Order System Step Response Plot

$$K_p = 5, K_d = 1, \gamma = 1, V = 1, \Delta T = 0.01$$



## Generating Locus Plots with Python

Finding closed-form solutions for  $\lambda_1, \lambda_2, \lambda_3$  is possible, but tedious.

Instead, we will generate the locus plots numerically with Python. A Google Colab notebook containing the code to generate the plots in the next few slides is available (here).



#### Case 1: Set $K_d = 0$

As a sanity check, let's generate the root locus plot when  $K_d = 0$ :



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#### Case 2: Set $K_d = 20$

With a non-zero  $K_d$ , we can see that now there is an optimal  $K_p$  value!



21 / 21