

6.3100: Dynamic System Modeling and Control Design

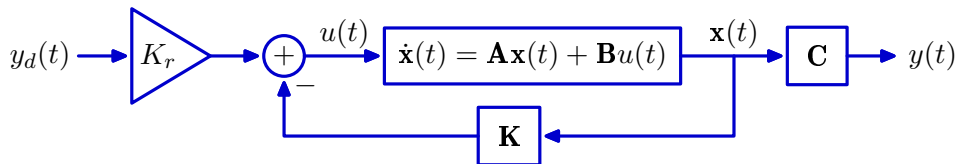
State-Space Responses

- Step Response
- Matrix Exponentials

State-Space Approach

Last week, we introduced the **State-Space** approach to control:

- Describe a system by its **states**.
- Describe dynamics of a system by **first-order** relations among states.
- Collect the states and relations in a single first-order **matrix** equation.



Plant: state matrix \mathbf{A} , input vector \mathbf{B} , and output vector \mathbf{C} :

$$\dot{\mathbf{x}}(t) = \mathbf{A}\mathbf{x}(t) + \mathbf{B}u(t)$$

$$y(t) = \mathbf{C}\mathbf{x}(t)$$

Feedback is characterized by a feedback vector \mathbf{K} and input scaler K_r :

$$u(t) = K_r y_d(t) - \mathbf{K}\mathbf{x}(t)$$

Combine to obtain **closed-loop** characterization:

$$\dot{\mathbf{x}}(t) = \left(\mathbf{A} - \mathbf{B}\mathbf{K} \right) \mathbf{x}(t) + \mathbf{B}\mathbf{K}_r y_d(t) \equiv \mathbf{A}_c \mathbf{x}(t) + \mathbf{B}_c y_d(t)$$

From State-Space to Transfer Function

Find the transfer function representation from the state-space description (similar to finding natural frequencies but $\mathbf{B}_c \neq 0$).

Start with the state equation:

$$\dot{\mathbf{x}}(t) = \mathbf{A}_c \mathbf{x}(t) + \mathbf{B}_c u(t)$$

Consider the input $u(t)$ and state $\mathbf{x}(t)$ at a particular complex frequency s :

$$u(t) = U(s)e^{st} \text{ and } \mathbf{x}(t) = \mathbf{X}(s)e^{st}$$

Find $H(s)$ at the same complex frequency.

$$s\mathbf{X}(s)e^{st} = \mathbf{A}_c \mathbf{X}(s)e^{st} + \mathbf{B}_c U(s)e^{st}$$

$$s\mathbf{X}(s) = \mathbf{A}_c \mathbf{X}(s) + \mathbf{B}_c U(s)$$

$$(s\mathbf{I} - \mathbf{A}_c)\mathbf{X}(s) = \mathbf{B}_c U(s)$$

$$\mathbf{X}(s) = (s\mathbf{I} - \mathbf{A}_c)^{-1} \mathbf{B}_c U(s)$$

$$Y(s) = \mathbf{C}_c \mathbf{X}(s) = \mathbf{C}_c (s\mathbf{I} - \mathbf{A}_c)^{-1} \mathbf{B}_c U(s)$$

$$H(s) = \frac{Y(s)}{U(s)} = \mathbf{C}_c (s\mathbf{I} - \mathbf{A}_c)^{-1} \mathbf{B}_c$$

From State-Space to Transfer Function

Example: find the open-loop transfer function

$$H(s) = \frac{Y(s)}{U(s)} = \mathbf{C}(s\mathbf{I} - \mathbf{A})^{-1}\mathbf{B}$$

for mass-spring-dashpot system.

$$\mathbf{A} = \begin{bmatrix} 0 & 1 \\ -k/m & -b/m \end{bmatrix} \quad \mathbf{B} = \begin{bmatrix} 0 \\ k/m \end{bmatrix} \quad \mathbf{C} = [1 \quad 0]$$

$$\begin{aligned} H(s) &= [1 \quad 0] \begin{bmatrix} s & -1 \\ k/m & s+b/m \end{bmatrix}^{-1} \begin{bmatrix} 0 \\ k/m \end{bmatrix} \\ &= [1 \quad 0] \frac{1}{s^2 + sb/m + k/m} \begin{bmatrix} s+b/m & 1 \\ -k/m & s \end{bmatrix} \begin{bmatrix} 0 \\ k/m \end{bmatrix} \\ &= \frac{1}{s^2 + sb/m + k/m} [s+b/m \quad 1] \begin{bmatrix} 0 \\ k/m \end{bmatrix} \\ &= \frac{k/m}{s^2 + sb/m + k/m} \quad \checkmark \end{aligned}$$

The denominator (and therefore poles) come from $|s\mathbf{I} - \mathbf{A}|$.

State-Space Analysis of Natural Frequencies

Are there frequencies s for which large outputs result when input $u(t)=0$?

$$H(s) = \frac{Y(s)}{X(s)} = \mathbf{C}_c(s\mathbf{I}-\mathbf{A})^{-1}\mathbf{B}_c = \mathbf{C}_c \frac{\text{adj}(s\mathbf{I}-\mathbf{A})}{|s\mathbf{I}-\mathbf{A}|} \mathbf{B}_c$$

If $|s\mathbf{I}-\mathbf{A}| = 0$, $H(s)$ is unbounded and therefore $|Y(s)| \rightarrow \infty$.

The natural frequencies are the solutions to the **characteristic equation**:

$$|s\mathbf{I}-\mathbf{A}_c| = 0$$

Example: mass-spring-dashpot system:

$$\mathbf{A}_c = \mathbf{A}-\mathbf{BK} = \begin{bmatrix} 0 & 1 \\ -k/m & -b/m \end{bmatrix} - \begin{bmatrix} 0 \\ k/m \end{bmatrix} [K_1 \quad K_2]$$

$$|s\mathbf{I}-\mathbf{A}_c| = \left| \begin{bmatrix} s & -1 \\ k(1+K_1)/m & s+(b+kK_2)/m \end{bmatrix} \right| = 0$$

Characteristic equation: $s^2 + (b+kK_2)s/m + k(1+K_1)/m = 0$ ✓

Check Yourself

A state-space controller is represented by the following equations:

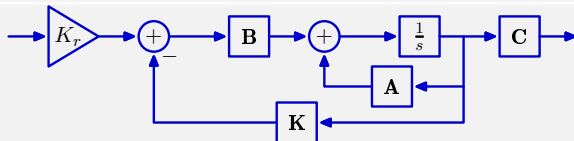
$$\dot{\mathbf{x}}(t) = \mathbf{A}\mathbf{x}(t) + \mathbf{B}u(t)$$

$$u(t) = K_r y_d(t) - \mathbf{K}\mathbf{x}(t)$$

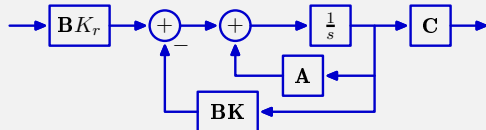
$$y(t) = \mathbf{C}\mathbf{x}(t)$$

Which block diagrams (below) correspond to the equations?

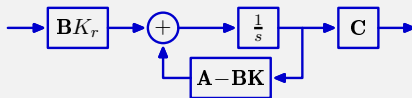
1.



2.



3.



Check Yourself

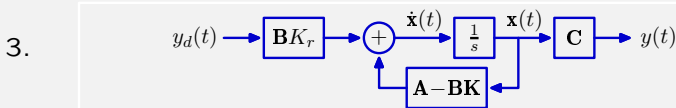
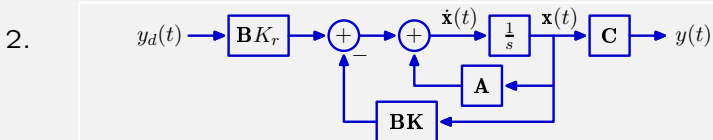
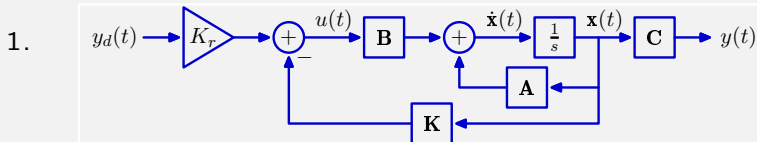
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$$\dot{\mathbf{x}}(t) = \mathbf{A}\mathbf{x}(t) + \mathbf{B}u(t)$$

$$u(t) = K_r y_d(t) - \mathbf{K}\mathbf{x}(t)$$

$$y(t) = \mathbf{C}\mathbf{x}(t)$$

Which block diagrams (below) correspond to the equations? **all**



Step Response

Find the step response $\mathbf{x}_s(t)$ of the following matrix system equation:

$$\dot{\mathbf{x}}(t) = \mathbf{P}\mathbf{x}(t) + \mathbf{Q}u(t)$$

Assume the initial value of the step response $\mathbf{x}_s(0) = \mathbf{0}$, and $u(t)=1$ for $t>0$.

Homogeneous equation: $\dot{\mathbf{x}}_h(t) = \mathbf{P}\mathbf{x}_h(t)$

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Homogeneous equation: $\dot{\mathbf{x}}_h(t) = \mathbf{P}\mathbf{x}_h(t)$

If this were a scalar equation:

$$\dot{x}_h(t) = px_h(t)$$

then the solution would be an exponential function of time:

$$x_h(t) = \alpha e^{pt}$$

Is there a matrix version of the exponential time function e^{pt} ?

Scalar Exponential Function

Exponential functions are eigenfunctions of the derivative operator:

$$e^{pt} \rightarrow \boxed{\frac{d}{dt}} \rightarrow pe^{pt}$$

Express the exponential function as a power series:

$$e^{pt} = 1 + \frac{pt}{1!} + \frac{p^2t^2}{2!} + \frac{p^3t^3}{3!} + \dots$$

Differentiate term-by-term:

$$\begin{aligned} \frac{d}{dt} e^{pt} &= 0 + \frac{p}{1!} + \frac{2p^2t}{2!} + \frac{3p^3t^2}{3!} + \dots \\ &= p + p \frac{pt}{1!} + p \frac{p^2t^2}{2!} + p \frac{p^3t^3}{3!} + \dots \\ &= p \left(1 + \frac{pt}{1!} + \frac{p^2t^2}{2!} + \frac{p^3t^3}{3!} + \dots \right) \\ &= pe^{pt} \quad \checkmark \end{aligned}$$

Matrix Exponential Function

Matrix exponentials are eigenfunctions of the matrix derivative operator:

$$e^{\mathbf{P}t} \rightarrow \boxed{\frac{d}{dt}} \rightarrow \mathbf{P}e^{\mathbf{P}t}$$

The matrix exponential function can also be expanded as a power series:

$$e^{\mathbf{P}t} = \mathbf{I} + \frac{\mathbf{P}t}{1!} + \frac{\mathbf{P}^2t^2}{2!} + \frac{\mathbf{P}^3t^3}{3!} + \dots$$

Differentiate term-by-term:

$$\begin{aligned} \frac{d}{dt}e^{\mathbf{P}t} &= 0 + \frac{\mathbf{P}}{1!} + \frac{2\mathbf{P}^2t}{2!} + \frac{3\mathbf{P}^3t^2}{3!} + \dots \\ &= \mathbf{P} + \mathbf{P}\frac{\mathbf{P}t}{1!} + \mathbf{P}\frac{\mathbf{P}^2t^2}{2!} + \mathbf{P}\frac{\mathbf{P}^3t^3}{3!} + \dots \\ &= \mathbf{P}\left(\mathbf{I} + \frac{\mathbf{P}t}{1!} + \frac{\mathbf{P}^2t^2}{2!} + \frac{\mathbf{P}^3t^3}{3!} + \dots\right) \\ &= \mathbf{P}e^{\mathbf{P}t} = e^{\mathbf{P}t}\mathbf{P} \quad \checkmark \end{aligned}$$

Step Response

Find the step response $\mathbf{x}_s(t)$ of the following matrix system equation:

$$\dot{\mathbf{x}}(t) = \mathbf{P}\mathbf{x}(t) + \mathbf{Q}u(t)$$

Assume the initial value of the step response $\mathbf{x}_s(0) = \mathbf{0}$, and $u(t)=1$ for $t>0$.

Homogeneous equation: $\dot{\mathbf{x}}_h(t) = \mathbf{P}\mathbf{x}_h(t)$

$$\mathbf{x}_h(t) = e^{\mathbf{P}t}\mathbf{\Psi}$$

Particular solution: $\mathbf{x}_p(t) = \mathbf{\Phi}$

$$\dot{\mathbf{x}}_p(t) = \mathbf{0} = \mathbf{P}\mathbf{\Phi} + \mathbf{Q}$$

$$\mathbf{\Phi} = -\mathbf{P}^{-1}\mathbf{Q} \quad (\text{provided that } \mathbf{P} \text{ is not singular})$$

Initial condition: $\mathbf{x}(0) = \mathbf{\Psi} - \mathbf{P}^{-1}\mathbf{Q} = \mathbf{0}$

$$\mathbf{\Psi} = \mathbf{P}^{-1}\mathbf{Q}$$

Step response:

$$\begin{aligned}\mathbf{x}_s(t) &= (e^{\mathbf{P}t} - \mathbf{I})\mathbf{P}^{-1}\mathbf{Q} \\ &= \mathbf{P}^{-1}(e^{\mathbf{P}t} - \mathbf{I})\mathbf{Q}\end{aligned}$$

Exponential functions play important role in solving matrix diff eq's.

Computing Matrix Exponentials

Finding the series expansion of a matrix exponential

$$e^{\mathbf{P}} = \mathbf{I} + \mathbf{P} + \mathbf{P}^2/2! + \mathbf{P}^3/3! + \mathbf{P}^4/4! + \dots$$

is easy when \mathbf{P} is **diagonal**:

$$\begin{aligned}\mathbf{P} &= \begin{bmatrix} \lambda_1 & & \\ & \lambda_2 & \\ & & \ddots \end{bmatrix} \\ e^{\mathbf{P}} &= \begin{bmatrix} 1 & & \\ & 1 & \\ & & \ddots \end{bmatrix} + \begin{bmatrix} \lambda_1 & & \\ & \lambda_2 & \\ & & \ddots \end{bmatrix} + \frac{1}{2!} \begin{bmatrix} \lambda_1 & & \\ & \lambda_2 & \\ & & \ddots \end{bmatrix}^2 + \dots \\ &= \begin{bmatrix} 1 & & \\ & 1 & \\ & & \ddots \end{bmatrix} + \begin{bmatrix} \lambda_1 & & \\ & \lambda_2 & \\ & & \ddots \end{bmatrix} + \frac{1}{2!} \begin{bmatrix} \lambda_1^2 & & \\ & \lambda_2^2 & \\ & & \ddots \end{bmatrix} + \dots \\ &= \begin{bmatrix} 1 + \lambda_1 + \lambda_1^2/2! + \dots & & \\ & 1 + \lambda_2 + \lambda_2^2/2! + \dots & \\ & & \ddots \end{bmatrix} = \begin{bmatrix} e^{\lambda_1} & & \\ & e^{\lambda_2} & \\ & & \ddots \end{bmatrix}\end{aligned}$$

Computing Matrix Exponentials

Fortunately it's easy to **diagonalize** a matrix that is full-rank and has distinct eigenvalues. Start with the eigenvector/eigenvalue property:

$$\mathbf{P}\mathbf{v}_i = \lambda_i\mathbf{v}_i \qquad \mathbf{v}_i \longrightarrow \boxed{\mathbf{P}} \longrightarrow \lambda_i\mathbf{v}_i$$

where λ_i is the i^{th} eigenvalue and \mathbf{v}_i is the i^{th} eigenvector (a column vector). If \mathbf{P} is full rank and if none of the eigenvalues are repeated

$$\begin{aligned}\mathbf{P}[\mathbf{v}_1|\mathbf{v}_2|\mathbf{v}_3|\cdots|\mathbf{v}_n] &= [\mathbf{P}\mathbf{v}_1|\mathbf{P}\mathbf{v}_2|\mathbf{P}\mathbf{v}_3|\cdots|\mathbf{P}\mathbf{v}_n] \\ &= [\lambda_1\mathbf{v}_1|\lambda_2\mathbf{v}_2|\lambda_3\mathbf{v}_3|\cdots|\lambda_n\mathbf{v}_n] \\ &= [\mathbf{v}_1|\mathbf{v}_2|\mathbf{v}_3|\cdots|\mathbf{v}_n] \begin{bmatrix} \lambda_1 & & & \\ & \lambda_2 & & \\ & & \ddots & \\ & & & \lambda_n \end{bmatrix}\end{aligned}$$

$$\mathbf{P}\mathbf{V} = \mathbf{V}\mathbf{\Lambda}$$

$$\mathbf{P} = \mathbf{V}\mathbf{\Lambda}\mathbf{V}^{-1}$$

where $\mathbf{V} = [\mathbf{v}_1|\mathbf{v}_2|\mathbf{v}_3|\cdots|\mathbf{v}_n]$ and $\mathbf{\Lambda} = \begin{bmatrix} \lambda_1 & & & \\ & \lambda_2 & & \\ & & \ddots & \\ & & & \lambda_n \end{bmatrix}$.

Computing Matrix Exponentials

Substitute the diagonal expansion of \mathbf{P} :

$$\mathbf{P} = \mathbf{V}\mathbf{\Lambda}\mathbf{V}^{-1}$$

into the series expansion of $e^{\mathbf{P}}$:

$$e^{\mathbf{P}} = \mathbf{I} + \mathbf{P} + \mathbf{P}^2/2! + \mathbf{P}^3/3! + \mathbf{P}^4/4! + \dots$$

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$$= \mathbf{I} + \boxed{\mathbf{V}\mathbf{\Lambda}\mathbf{V}^{-1}} + \frac{1}{2!} \boxed{\mathbf{V}\mathbf{\Lambda}\mathbf{V}^{-1}} \boxed{\mathbf{V}\mathbf{\Lambda}\mathbf{V}^{-1}} + \frac{1}{3!} \boxed{\mathbf{V}\mathbf{\Lambda}\mathbf{V}^{-1}} \boxed{\mathbf{V}\mathbf{\Lambda}\mathbf{V}^{-1}} \boxed{\mathbf{V}\mathbf{\Lambda}\mathbf{V}^{-1}} + \dots$$

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$$= \mathbf{I} + \boxed{\mathbf{V}\mathbf{\Lambda}\mathbf{V}^{-1}} + \frac{1}{2!} \boxed{\mathbf{V}\mathbf{\Lambda}\mathbf{V}^{-1}} \boxed{\mathbf{V}\mathbf{\Lambda}\mathbf{V}^{-1}} + \frac{1}{3!} \boxed{\mathbf{V}\mathbf{\Lambda}\mathbf{V}^{-1}} \boxed{\mathbf{V}\mathbf{\Lambda}\mathbf{V}^{-1}} \boxed{\mathbf{V}\mathbf{\Lambda}\mathbf{V}^{-1}} + \dots$$

$$= \mathbf{I} + \mathbf{V}\mathbf{\Lambda}\mathbf{V}^{-1} + \frac{1}{2!} \mathbf{V}\mathbf{\Lambda} \boxed{\mathbf{V}^{-1}\mathbf{V}} \mathbf{\Lambda}\mathbf{V}^{-1} + \frac{1}{3!} \mathbf{V}\mathbf{\Lambda} \boxed{\mathbf{V}^{-1}\mathbf{V}} \mathbf{\Lambda} \boxed{\mathbf{V}^{-1}\mathbf{V}} \mathbf{\Lambda}\mathbf{V}^{-1} + \dots$$

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Substitute the diagonal expansion of \mathbf{P} :

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$$= \mathbf{I} + \mathbf{V}\mathbf{\Lambda}\mathbf{V}^{-1} + \frac{1}{2!} \mathbf{V}\mathbf{\Lambda} \boxed{\mathbf{V}^{-1}\mathbf{V}} \mathbf{\Lambda}\mathbf{V}^{-1} + \frac{1}{3!} \mathbf{V}\mathbf{\Lambda} \boxed{\mathbf{V}^{-1}\mathbf{V}} \mathbf{\Lambda} \boxed{\mathbf{V}^{-1}\mathbf{V}} \mathbf{\Lambda}\mathbf{V}^{-1} + \dots$$

$$= \mathbf{I} + \mathbf{V}\mathbf{\Lambda}\mathbf{V}^{-1} + \frac{1}{2!} \mathbf{V}\mathbf{\Lambda}^2\mathbf{V}^{-1} + \frac{1}{3!} \mathbf{V}\mathbf{\Lambda}^3\mathbf{V}^{-1} + \dots$$

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Substitute the diagonal expansion of \mathbf{P} :

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$$= \mathbf{I} + \mathbf{V}\mathbf{\Lambda}\mathbf{V}^{-1} + \frac{1}{2!} \mathbf{V}\mathbf{\Lambda} \boxed{\mathbf{V}^{-1}\mathbf{V}} \mathbf{\Lambda}\mathbf{V}^{-1} + \frac{1}{3!} \mathbf{V}\mathbf{\Lambda} \boxed{\mathbf{V}^{-1}\mathbf{V}} \mathbf{\Lambda} \boxed{\mathbf{V}^{-1}\mathbf{V}} \mathbf{\Lambda}\mathbf{V}^{-1} + \dots$$

$$= \mathbf{I} + \mathbf{V}\mathbf{\Lambda}\mathbf{V}^{-1} + \frac{1}{2!} \mathbf{V}\mathbf{\Lambda}^2\mathbf{V}^{-1} + \frac{1}{3!} \mathbf{V}\mathbf{\Lambda}^3\mathbf{V}^{-1} + \dots$$

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Substitute the diagonal expansion of \mathbf{P} :

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$$= \mathbf{V} \left(\mathbf{I} + \mathbf{\Lambda} + \frac{1}{2!} \mathbf{\Lambda}^2 + \frac{1}{3!} \mathbf{\Lambda}^3 + \dots \right) \mathbf{V}^{-1}$$

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Substitute the diagonal expansion of \mathbf{P} :

$$\mathbf{P} = \mathbf{V}\mathbf{\Lambda}\mathbf{V}^{-1}$$

into the series expansion of $e^{\mathbf{P}}$:

$$e^{\mathbf{P}} = \mathbf{I} + \mathbf{P} + \frac{\mathbf{P}^2}{2!} + \frac{\mathbf{P}^3}{3!} + \frac{\mathbf{P}^4}{4!} + \dots$$

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$$= \mathbf{I} + \mathbf{V}\mathbf{\Lambda}\mathbf{V}^{-1} + \frac{1}{2!} \mathbf{V}\mathbf{\Lambda}^2\mathbf{V}^{-1} + \frac{1}{3!} \mathbf{V}\mathbf{\Lambda}^3\mathbf{V}^{-1} + \dots$$

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$$= \mathbf{V} \left(\mathbf{I} + \mathbf{\Lambda} + \frac{1}{2!} \mathbf{\Lambda}^2 + \frac{1}{3!} \mathbf{\Lambda}^3 + \dots \right) \mathbf{V}^{-1}$$

$$= \mathbf{V}e^{\mathbf{\Lambda}}\mathbf{V}^{-1}$$

The matrix exponential of \mathbf{P} can be directly computed from the eigenvalues and eigenvectors of \mathbf{P} .

Computing Matrix Exponentials: Example

Determine $e^{\mathbf{P}t}$ for $\mathbf{P} = \begin{bmatrix} 0 & 1 \\ -2 & -3 \end{bmatrix}$.

Step 1: Find the eigenvalues of \mathbf{P} .

Computing Matrix Exponentials: Example

Determine $e^{\mathbf{P}t}$ for $\mathbf{P} = \begin{bmatrix} 0 & 1 \\ -2 & -3 \end{bmatrix}$.

Step 1: Find the eigenvalues of \mathbf{P} .

$$|s\mathbf{I} - \mathbf{P}| = \left| \begin{bmatrix} s & -1 \\ 2 & s+3 \end{bmatrix} \right| = s^2 + 3s + 2 = (s+1)(s+2) = 0$$

$$s_{1,2} = -1, -2$$

Computing Matrix Exponentials: Example

Determine $e^{\mathbf{P}t}$ for $\mathbf{P} = \begin{bmatrix} 0 & 1 \\ -2 & -3 \end{bmatrix}$.

Step 1: Find the eigenvalues of \mathbf{P} : -1 and -2 .

Step 2: Find the eigenvectors of \mathbf{P}

$$\mathbf{P}\mathbf{v} = \mathbf{P} \begin{bmatrix} a \\ b \end{bmatrix} = s\mathbf{v} = s \begin{bmatrix} a \\ b \end{bmatrix}$$

Computing Matrix Exponentials: Example

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$$\mathbf{P}\mathbf{v} = \mathbf{P} \begin{bmatrix} a \\ b \end{bmatrix} = s\mathbf{v} = s \begin{bmatrix} a \\ b \end{bmatrix}$$

$s = -1$:

$$\begin{bmatrix} 0 & 1 \\ -2 & -3 \end{bmatrix} \begin{bmatrix} a \\ b \end{bmatrix} = -1 \begin{bmatrix} a \\ b \end{bmatrix}$$

$$b = -a$$

$$-2a - 3b = -b$$

$$\begin{bmatrix} a \\ b \end{bmatrix} = \alpha \begin{bmatrix} 1 \\ -1 \end{bmatrix}; \forall \alpha$$

Computing Matrix Exponentials: Example

Determine $e^{\mathbf{P}t}$ for $\mathbf{P} = \begin{bmatrix} 0 & 1 \\ -2 & -3 \end{bmatrix}$.

Step 1: Find the eigenvalues of \mathbf{P} : -1 and -2 .

Step 2: Find the eigenvectors of \mathbf{P}

$$\mathbf{P}\mathbf{v} = \mathbf{P} \begin{bmatrix} a \\ b \end{bmatrix} = s\mathbf{v} = s \begin{bmatrix} a \\ b \end{bmatrix}$$

$s = -2$:

$$\begin{bmatrix} 0 & 1 \\ -2 & -3 \end{bmatrix} \begin{bmatrix} a \\ b \end{bmatrix} = -2 \begin{bmatrix} a \\ b \end{bmatrix}$$

$$b = -2a$$

$$-2a - 3b = -2b$$

$$\begin{bmatrix} a \\ b \end{bmatrix} = \beta \begin{bmatrix} 1 \\ -2 \end{bmatrix}; \quad \forall \beta$$

Computing Matrix Exponentials: Example

Determine $e^{\mathbf{P}t}$ for $\mathbf{P} = \begin{bmatrix} 0 & 1 \\ -2 & -3 \end{bmatrix}$.

Step 1: Find the eigenvalues of \mathbf{P} : -1 and -2 .

Step 2: Find the eigenvectors of \mathbf{P} : $\begin{bmatrix} 1 \\ -1 \end{bmatrix}$ and $\begin{bmatrix} 1 \\ -2 \end{bmatrix}$.

Computing Matrix Exponentials: Example

Determine $e^{\mathbf{P}t}$ for $\mathbf{P} = \begin{bmatrix} 0 & 1 \\ -2 & -3 \end{bmatrix}$.

Step 1: Find the eigenvalues of \mathbf{P} : -1 and -2 .

Step 2: Find the eigenvectors of \mathbf{P} : $\begin{bmatrix} 1 \\ -1 \end{bmatrix}$ and $\begin{bmatrix} 1 \\ -2 \end{bmatrix}$.

Step 3: Find $e^{\mathbf{P}t} = \mathbf{V}e^{\mathbf{\Lambda}t}\mathbf{V}^{-1}$.

$$\begin{aligned} e^{\mathbf{P}t} &= \left[\begin{array}{c|c} 1 & 1 \\ -1 & -2 \end{array} \right] \begin{bmatrix} e^{-t} & 0 \\ 0 & e^{-2t} \end{bmatrix} \left[\begin{array}{c|c} 1 & 1 \\ -1 & -2 \end{array} \right]^{-1} \\ &= \begin{bmatrix} 1 & 1 \\ -1 & -2 \end{bmatrix} \begin{bmatrix} e^{-t} & 0 \\ 0 & e^{-2t} \end{bmatrix} \begin{bmatrix} 2 & 1 \\ -1 & -1 \end{bmatrix} \\ &= \begin{bmatrix} e^{-t} & e^{-2t} \\ -e^{-t} & -2e^{-2t} \end{bmatrix} \begin{bmatrix} 2 & 1 \\ -1 & -1 \end{bmatrix} \\ &= \begin{bmatrix} 2e^{-t} - e^{-2t} & e^{-t} - e^{-2t} \\ -2e^{-t} + 2e^{-2t} & -e^{-t} + 2e^{-2t} \end{bmatrix} \end{aligned}$$

Check Yourself

Let

$$\mathbf{P} = \begin{bmatrix} 0 & 1 \\ -1 & 0 \end{bmatrix}$$

Which of the following matrices equals $e^{\mathbf{P}t}$?

1. $\begin{bmatrix} e^{jt} & e^{-jt} \\ e^{-jt} & e^{jt} \end{bmatrix}$

2. $\begin{bmatrix} \cos(t) & \sin(t) \\ -\sin(t) & \cos(t) \end{bmatrix}$

3. $\begin{bmatrix} e^t & e^{-t} \\ e^{-t} & e^t \end{bmatrix}$

4. $\begin{bmatrix} te^t & te^{-t} \\ te^{-t} & te^t \end{bmatrix}$

5. none of the above

Check Yourself

Let

$$\mathbf{P} = \begin{bmatrix} 0 & 1 \\ -1 & 0 \end{bmatrix}$$

Determine $e^{\mathbf{P}t}$

Step 1: Find the eigenvalues of \mathbf{P} .

$$|s\mathbf{I} - \mathbf{P}| = 0$$

$$\left| \begin{bmatrix} s & 0 \\ 0 & s \end{bmatrix} - \begin{bmatrix} 0 & 1 \\ -1 & 0 \end{bmatrix} \right| = \left| \begin{bmatrix} s & -1 \\ 1 & s \end{bmatrix} \right| = s^2 + 1 = 0$$

$$s_{1,2} = \pm j$$

Check Yourself

Let

$$\mathbf{P} = \begin{bmatrix} 0 & 1 \\ -1 & 0 \end{bmatrix}$$

Determine $e^{\mathbf{P}t}$

Step 1: Find the eigenvalues of \mathbf{P} : $s_{1,2} = \pm j$

Step 2: Find the eigenvectors of \mathbf{P} .

Check Yourself

Let

$$\mathbf{P} = \begin{bmatrix} 0 & 1 \\ -1 & 0 \end{bmatrix}$$

Determine $e^{\mathbf{P}t}$

Step 1: Find the eigenvalues of \mathbf{P} : $s_{1,2} = \pm j$

Step 2: Find the eigenvectors of \mathbf{P}

$$\mathbf{P}\mathbf{v} = s\mathbf{v}$$

$$\begin{bmatrix} 0 & 1 \\ -1 & 0 \end{bmatrix} \begin{bmatrix} a \\ b \end{bmatrix} = j \begin{bmatrix} a \\ b \end{bmatrix}$$

$$b = ja$$

$$-a = jb$$

The second equation is j times the first. The eigenvector can be taken as any scalar multiple of $\begin{bmatrix} 1 \\ j \end{bmatrix}$

Check Yourself

Let

$$\mathbf{P} = \begin{bmatrix} 0 & 1 \\ -1 & 0 \end{bmatrix}$$

Determine $e^{\mathbf{P}t}$

Step 1: Find the eigenvalues of \mathbf{P} : $s_{1,2} = \pm j$

Step 2: Find the eigenvectors of \mathbf{P}

$$\mathbf{P}\mathbf{v} = s\mathbf{v}$$

$$\begin{bmatrix} 0 & 1 \\ -1 & 0 \end{bmatrix} \begin{bmatrix} a \\ b \end{bmatrix} = -j \begin{bmatrix} a \\ b \end{bmatrix}$$

$$b = -ja$$

$$-a = -jb$$

The second equation is $-j$ times the first. The eigenvector can be taken as any scalar multiple of $\begin{bmatrix} 1 \\ -j \end{bmatrix}$

Check Yourself

Let

$$\mathbf{P} = \begin{bmatrix} 0 & 1 \\ -1 & 0 \end{bmatrix}$$

Determine $e^{\mathbf{P}t}$

Step 1: Find the eigenvalues of \mathbf{P} : $s_{1,2} = \pm j$

Step 2: Find the eigenvectors of \mathbf{P} : $\begin{bmatrix} 1 \\ j \end{bmatrix}$ and $\begin{bmatrix} 1 \\ -j \end{bmatrix}$.

Step 3: Calculate the complex exponential.

Check Yourself

Let

$$\mathbf{P} = \begin{bmatrix} 0 & 1 \\ -1 & 0 \end{bmatrix}$$

Determine $e^{\mathbf{P}t}$

Step 1: Find the eigenvalues of \mathbf{P} : $s_{1,2} = \pm j$

Step 2: Find the eigenvectors of \mathbf{P} : $\begin{bmatrix} 1 \\ j \end{bmatrix}$ and $\begin{bmatrix} 1 \\ -j \end{bmatrix}$.

Step 3: Calculate the complex exponential.

$$\begin{aligned} e^{\mathbf{P}t} &= \mathbf{V}e^{\mathbf{\Lambda}t}\mathbf{V}^{-1} = \begin{bmatrix} 1 & 1 \\ j & -j \end{bmatrix} \begin{bmatrix} e^{jt} & 0 \\ 0 & e^{-jt} \end{bmatrix} \begin{bmatrix} 1/2 & -j/2 \\ 1/2 & j/2 \end{bmatrix} \\ &= \begin{bmatrix} e^{jt} & e^{-jt} \\ je^{jt} & -je^{-jt} \end{bmatrix} \begin{bmatrix} 1/2 & -j/2 \\ 1/2 & j/2 \end{bmatrix} = \begin{bmatrix} (e^{jt}+e^{-jt})/2 & -j(e^{jt}-e^{-jt})/2 \\ j(e^{jt}-e^{-jt})/2 & (e^{jt}+e^{-jt})/2 \end{bmatrix} \\ &= \begin{bmatrix} \cos(t) & \sin(t) \\ -\sin(t) & \cos(t) \end{bmatrix} \end{aligned}$$

Check Yourself

Let

$$\mathbf{P} = \begin{bmatrix} 0 & 1 \\ -1 & 0 \end{bmatrix}$$

Which of the following matrices equals $e^{\mathbf{P}t}$? 2

1. $\begin{bmatrix} e^{jt} & e^{-jt} \\ e^{-jt} & e^{jt} \end{bmatrix}$

2. $\begin{bmatrix} \cos(t) & \sin(t) \\ -\sin(t) & \cos(t) \end{bmatrix}$

3. $\begin{bmatrix} e^t & e^{-t} \\ e^{-t} & e^t \end{bmatrix}$

4. $\begin{bmatrix} te^t & te^{-t} \\ te^{-t} & te^t \end{bmatrix}$

5. none of the above

Check Yourself

Let

$$\mathbf{P} = \begin{bmatrix} 0 & 1 \\ -1 & 0 \end{bmatrix}$$

Determine $e^{\mathbf{P}t}$

Alternative method: use series expansion

$$\begin{aligned} e^{\mathbf{P}t} &= \mathbf{I} + \frac{\mathbf{P}t}{1!} + \frac{\mathbf{P}^2 t^2}{2!} + \frac{\mathbf{P}^3 t^3}{3!} + \frac{\mathbf{P}^4 t^4}{4!} + \dots \\ &= \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} + \begin{bmatrix} 0 & 1 \\ -1 & 0 \end{bmatrix} t + \begin{bmatrix} -1 & 0 \\ 0 & -1 \end{bmatrix} \frac{t^2}{2!} + \begin{bmatrix} 0 & -1 \\ 1 & 0 \end{bmatrix} \frac{t^3}{3!} + \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} \frac{t^4}{4!} + \dots \\ &= \begin{bmatrix} 1 - \frac{t^2}{2!} + \frac{t^4}{4!} - \frac{t^6}{6!} + \frac{t^8}{8!} - + \dots & t - \frac{t^3}{3!} + \frac{t^5}{5!} - \frac{t^7}{7!} + \frac{t^9}{9!} - + \dots \\ -t + \frac{t^3}{3!} - \frac{t^5}{5!} + \frac{t^7}{7!} - \frac{t^9}{9!} \dots & 1 - \frac{t^2}{2!} + \frac{t^4}{4!} - \frac{t^6}{6!} + \frac{t^8}{8!} - + \dots \end{bmatrix} \\ &= \begin{bmatrix} \cos(t) & \sin(t) \\ -\sin(t) & \cos(t) \end{bmatrix} \end{aligned}$$

Compare Methods

Let

$$\mathbf{P} = \begin{bmatrix} 0 & 1 \\ -1 & 0 \end{bmatrix}$$

Determine $e^{\mathbf{P}t}$

Series method requires closing infinite sums. ✗

$$\begin{aligned} e^{\mathbf{P}t} &= \mathbf{I} + \frac{\mathbf{P}t}{1!} + \frac{\mathbf{P}^2 t^2}{2!} + \frac{\mathbf{P}^3 t^3}{3!} + \frac{\mathbf{P}^4 t^4}{4!} + \dots \\ &= \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} + \begin{bmatrix} 0 & 1 \\ -1 & 0 \end{bmatrix} t + \begin{bmatrix} -1 & 0 \\ 0 & -1 \end{bmatrix} \frac{t^2}{2!} + \begin{bmatrix} 0 & -1 \\ 1 & 0 \end{bmatrix} \frac{t^3}{3!} + \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} \frac{t^4}{4!} + \dots \\ &= \begin{bmatrix} 1 - \frac{t^2}{2!} + \frac{t^4}{4!} - \frac{t^6}{6!} + \frac{t^8}{8!} - + \dots & t - \frac{t^3}{3!} + \frac{t^5}{5!} - \frac{t^7}{7!} + \frac{t^9}{9!} - + \dots \\ -t + \frac{t^3}{3!} - \frac{t^5}{5!} + \frac{t^7}{7!} - \frac{t^9}{9!} \dots & 1 - \frac{t^2}{2!} + \frac{t^4}{4!} - \frac{t^6}{6!} + \frac{t^8}{8!} - + \dots \end{bmatrix} \\ &= \begin{bmatrix} \cos(t) & \sin(t) \\ -\sin(t) & \cos(t) \end{bmatrix} \end{aligned}$$

Check Yourself

Let

$$\mathbf{P} = \begin{bmatrix} 0 & 1 \\ -1 & 0 \end{bmatrix}$$

Determine $e^{\mathbf{P}t}$

The diagonalizing method uses conventional linear algebra. ✓

Step 1: Find the eigenvalues \mathbf{P} : $s_{1,2} = \pm j$

Step 2: Find the eigenvectors of \mathbf{P} : $\begin{bmatrix} 1 \\ j \end{bmatrix}$ and $\begin{bmatrix} 1 \\ -j \end{bmatrix}$.

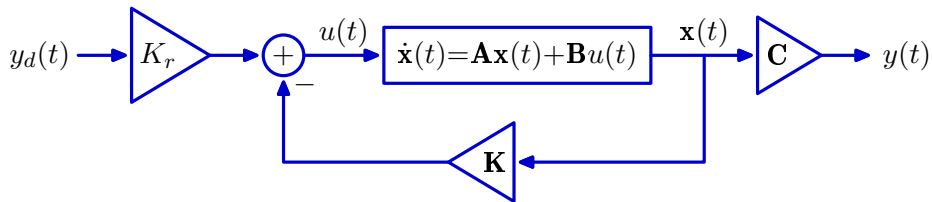
Step 3: Calculate the complex exponential $e^{\mathbf{P}t} = \mathbf{V}e^{\mathbf{\Lambda}t}\mathbf{V}^{-1}$

- assemble \mathbf{V} = matrix of eigenvectors
- assemble $e^{\mathbf{\Lambda}t}$ = matrix of eigenfunctions
- determine the inverse of \mathbf{V}
- matrix multiply

Easily done with numerical methods in Python, MATLAB, ...

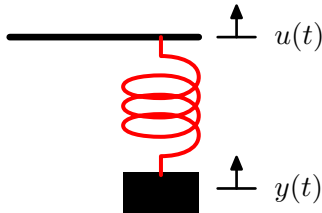
Controller Design

Optimizing the gains \mathbf{K} and K_r of a state-space controller.



Controlling a Mass-Spring-Dashpot

Start by reviewing how we chose gains for a classical controller.



Model the mass-spring-dashpot system (Newton's Law):

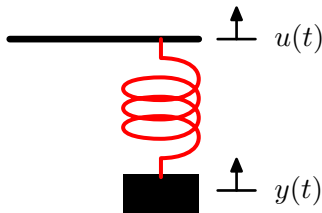
$$\underbrace{k(x(t)-y(t))}_{F} - \underbrace{by(t)}_{ma} = m\ddot{y}(t)$$

to get the (open loop) transfer function of the plant:

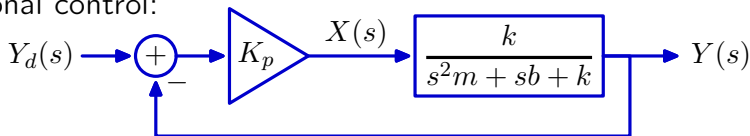
$$G(s) = \frac{Y(s)}{X(s)} = \frac{k}{s^2m + sb + k}$$

Proportional Control of a Mass-Spring-Dashpot

Start by reviewing how we chose gains for a classical controller.



Proportional control:

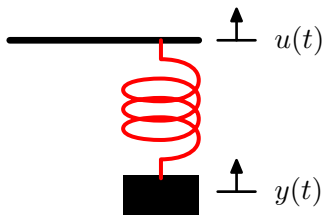


Closed-loop transfer function:

$$H(s) = \frac{Y(s)}{Y_d(s)} = \frac{kK_p}{s^2 m + s b + k(1+K_p)}$$

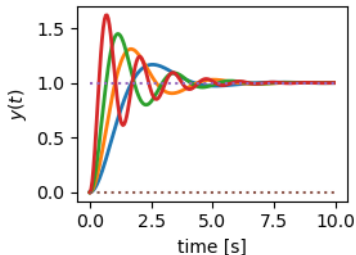
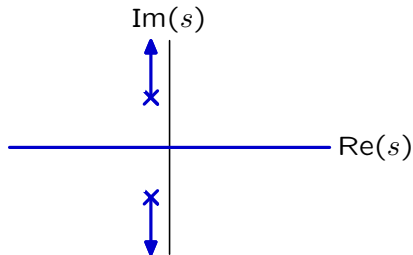
Closed-loop poles are roots of denominator: $s_{1,2} = \frac{-b \pm \sqrt{b^2 - 4mk(1+K_p)}}{2m}$

Root-Locus Analysis of Proportional Control



Consider the closed-loop poles $s_1, s_2 = \frac{-b \pm \sqrt{b^2 - 4mk(1+K_p)}}{2m}$

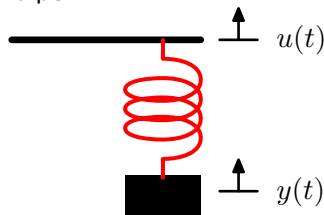
when $m = 1$, $b = 1.4$, $k = 2$, and K_p increases from 0 to ∞ .



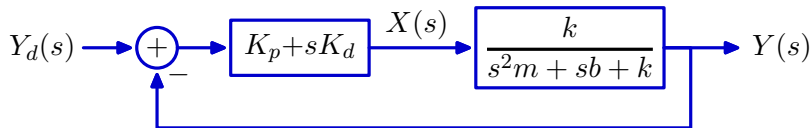
As $K_p \uparrow$, frequency of ringing \uparrow , but peaks decay with same time constant.

Proportional Plus Derivative Control

Adding a derivative term helps.



Same open-loop transfer function, different controller:



Closed-loop transfer function:

$$H(s) = \frac{Y(s)}{Y_d(s)} = \frac{k(K_p + sK_d)}{s^2m + s(b + kK_d) + k(1 + K_p)}$$

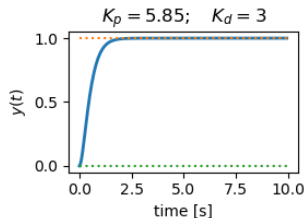
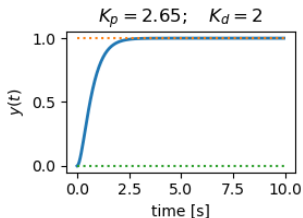
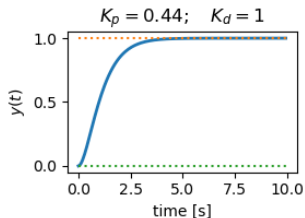
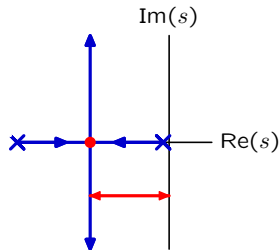
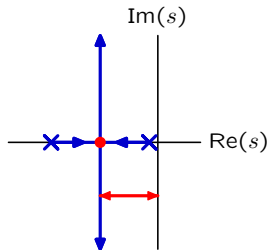
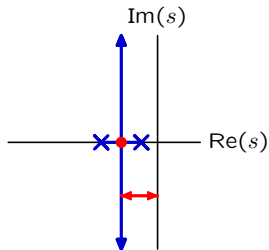
$$\text{Closed-loop poles: } s = \frac{-b - kK_d \pm \sqrt{(b + kK_d)^2 - 4mk(1 + K_p)}}{2m}$$

Root-Locus Analysis of PD Control

Increasing K_d enables faster closed-loop poles (red dots) without overshoot.

$$s = \frac{-b - kK_d \pm \sqrt{(b + kK_d)^2 - 4mk(1 + K_p)}}{2m}$$

$m = 1$; $b = 1.4$; $k = 2$; $K_d = 1, 2, 3$; $K_p: 0 \rightarrow \infty$.



More Advanced Methods in Classical Control

Derivative feedback is just one way to optimize a classical controller.

Other advanced classical methods include

- integral feedback for PID control,
- optimizing gain and phase margins,
- lead compensation, lag compensation, lead/lag compensation, and
- many other techniques.

Much of the design power of these advanced methods results from their ability to **move poles and zeros** to locations that are more favorable for

- stability,
- disturbance rejection,
- noise immunity, etc.

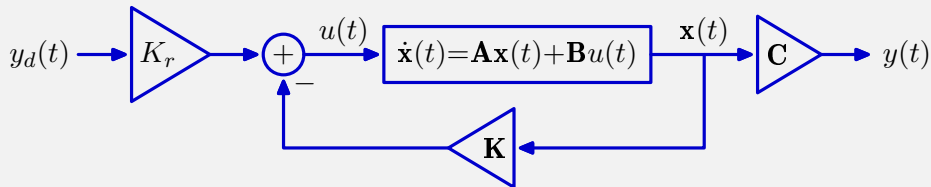
We can similarly optimize state-space controllers.

And the state-space formulation is much more powerful!

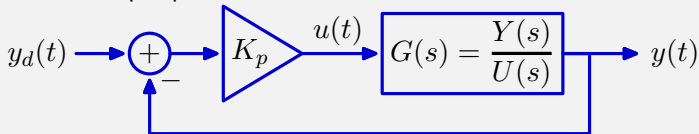
Stopped Here

Check Yourself: Proportional Control in State Space

Choose \mathbf{K} and K_r so that the state-space controller:



is equivalent to a proportional controller:

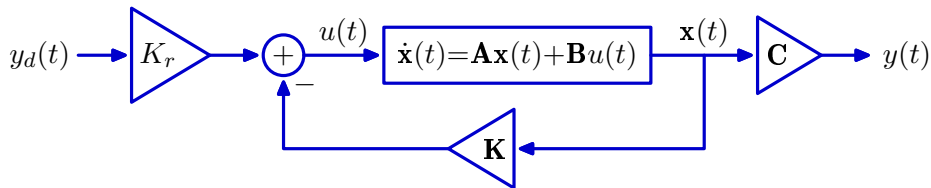


What \mathbf{K} and K_r implement a proportional controller?

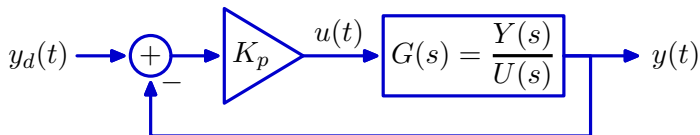
1. $\mathbf{K} = K_r \mathbf{C}$ and $K_r = K_p$
2. $\mathbf{K} = \mathbf{C}\mathbf{B}$ and $K_r = 1$
3. $\mathbf{K} = \mathbf{C}$ and $K_r = K_p$
4. $\mathbf{K} = K_p \mathbf{C}$ and $K_r = K_p$
5. none of the above

Check Yourself: Proportional Control in State Space

Choose \mathbf{K} and K_r so that the state-space controller:



is equivalent to a proportional controller:



To be equivalent, the controllers must produce the same plant input $u(t)$:

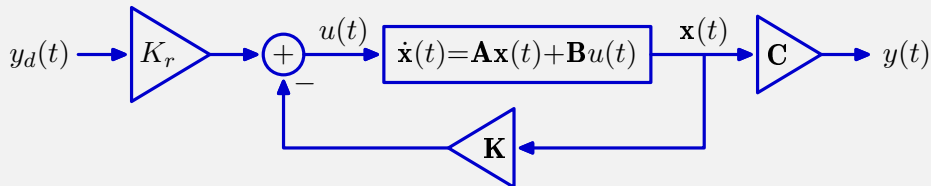
$$\begin{aligned}u(t) &= K_r y_d(t) - \mathbf{K} \mathbf{x}(t) = K_p (y_d(t) - y(t)) \\ &= K_p y_d(t) - K_p \mathbf{C} \mathbf{x}(t)\end{aligned}$$

$$K_r = K_p$$

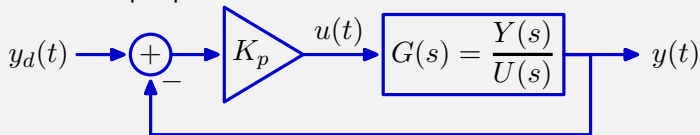
$$\mathbf{K} = K_p \mathbf{C}$$

Check Yourself: Proportional Control in State Space

Choose \mathbf{K} and K_r so that the state-space controller:



is equivalent to a proportional controller:

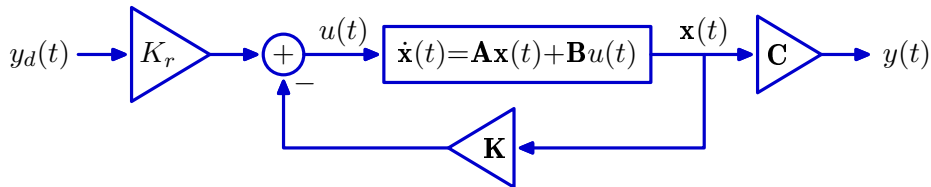


What \mathbf{K} and K_r implement a proportional controller? 4.

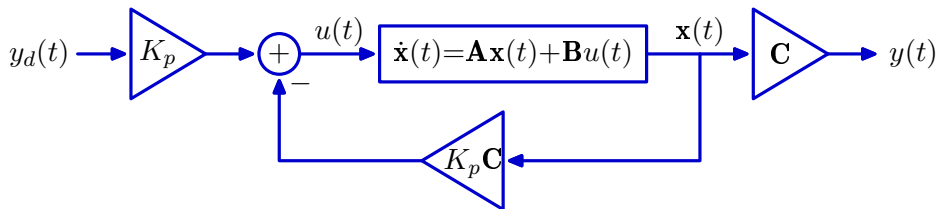
1. $\mathbf{K} = K_r \mathbf{C}$ and $K_r = K_p$
2. $\mathbf{K} = \mathbf{C}\mathbf{B}$ and $K_r = 1$
3. $\mathbf{K} = \mathbf{C}$ and $K_r = K_p$
4. $\mathbf{K} = K_p \mathbf{C}$ and $K_r = K_p$
5. none of the above

Proportional Control with State-Space Model

We can implement **proportional control** with a state-space model



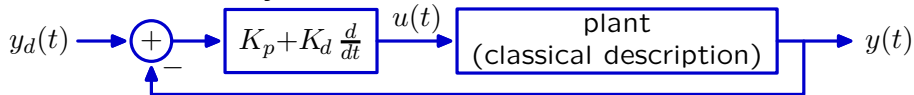
by setting $\mathbf{K} = K_p \mathbf{C}$ and $K_r = K_p$:



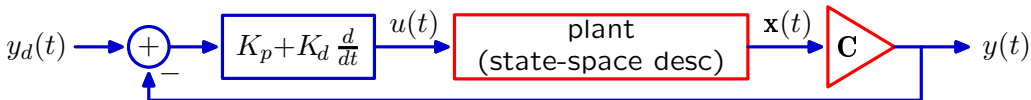
We can also implement **proportional plus derivative control** with a state-space model.

Proportional Plus Derivative Control in State-Space

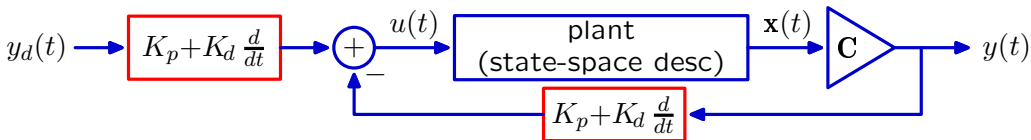
Start with a classical system with PD control:



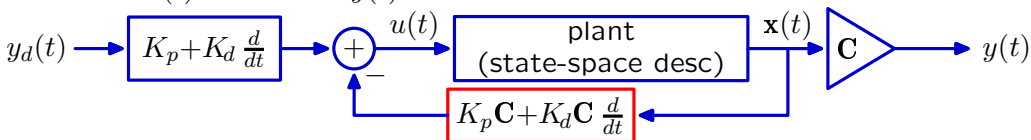
Replace classical description of plant with equiv. state-space description:



Distribute the PD controller over the inputs to the subtractor:



Feedback $\mathbf{x}(t)$ instead of $y(t)$:



Result is a state-space controller with $K_r = K_p + K_d \frac{d}{dt}$ and $\mathbf{K} = K_p \mathbf{C} + K_d \mathbf{C} \frac{d}{dt}$.

More Advanced Methods in Classical Control

Much of the design power of the more advanced methods results from their ability to **move poles and zeros** to locations that are more favorable for

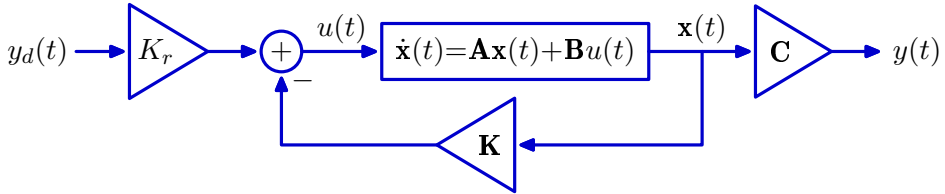
- stability,
- disturbance rejection,
- noise immunity, etc.

We can similarly optimize state-space controllers.

And the state-space formulation is much more powerful!

Pole Placement

With the correct choice of gains \mathbf{K} and K_r , we can move the closed-loop poles of a state-space model **anywhere** in the complex plane.



The closed-loop poles of a state-space model are equal to the roots of its characteristic polynomial:

$$\left| s\mathbf{I} - (\mathbf{A} - \mathbf{B}\mathbf{K}) \right| = 0$$

Fundamental theorem of algebra: an n^{th} order polynomial has n roots.

Factor theorem: each root determines a first-order factor.

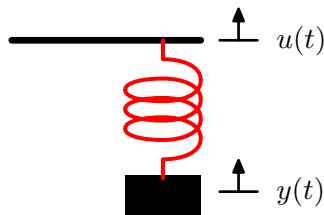
→ characteristic polynomial can be written as a product of first-order terms:

$$\left| s\mathbf{I} - (\mathbf{A} - \mathbf{B}\mathbf{K}) \right| = \prod_{i=1}^n (s - s_i) = 0$$

LHS: n^{th} order polynomial in s (pole locations)

RHS: same polynomial, but coeff's in terms of desired pole locations s_i .

Example: Pole Placement for Mass-Spring-Dashpot



Plant:

$$\underbrace{k(u(t)-y(t))}_F - \underbrace{b\dot{y}(t)}_{ma} = m\ddot{y}(t)$$

Rewrite this second-order differential equation as two **first-order** equations:

$$\underbrace{\frac{d}{dt} \begin{bmatrix} y(t) \\ \dot{y}(t) \end{bmatrix}}_{\dot{\mathbf{x}}(t)} = \underbrace{\begin{bmatrix} 0 & 1 \\ -k/m & -b/m \end{bmatrix}}_{\mathbf{A}} \underbrace{\begin{bmatrix} y(t) \\ \dot{y}(t) \end{bmatrix}}_{\mathbf{x}(t)} + \underbrace{\begin{bmatrix} 0 \\ k/m \end{bmatrix}}_{\mathbf{B}} u(t)$$

which can be expressed as a single matrix equation:

$$\dot{\mathbf{x}}(t) = \mathbf{A}\mathbf{x}(t) + \mathbf{B}u(t)$$

Example: Pole Placement for Mass-Spring-Dashpot

For $m = 1$, $b = 1.4$, and $k = 2$:

$$\mathbf{A} = \begin{bmatrix} 0 & 1 \\ -2 & -1.4 \end{bmatrix} \quad \mathbf{B} = \begin{bmatrix} 0 \\ 2 \end{bmatrix}$$

With $\mathbf{K} = [k_1 \quad k_2]$:

$$|s\mathbf{I} - (\mathbf{A} - \mathbf{BK})| = \left| \begin{bmatrix} s & -1 \\ 2+2k_1 & s+1.4+2k_2 \end{bmatrix} \right| = s^2 + (1.4+2k_2)s + (2+2k_1)$$

To place poles at $s = -0.5$ and $s = -1$, set

$$s^2 + (1.4+2k_2)s + (2+2k_1) = (s+0.5)(s+1) = s^2 + 1.5s + 0.5$$

$\rightarrow k_1 = -0.75$ and $k_2 = 0.05$.

Alternatively, to place poles at $s = -0.5$ and $s = -0.6$, set

$$s^2 + (1.4+2k_2)s + (2+2k_1) = (s+0.5)(s+0.6) = s^2 + 1.1s + 0.3$$

$\rightarrow k_1 = -0.85$ and $k_2 = -0.15$.

Check Yourself

Let \mathbf{A} represent the system matrix and \mathbf{B} represent the input matrix for a state-space control system, where these matrices are given by

$$\mathbf{A} = \begin{bmatrix} 1 & 1 \\ 0 & 1 \end{bmatrix} \quad \mathbf{B} = \begin{bmatrix} 0 \\ 1 \end{bmatrix}$$

Which \mathbf{K} vector will produce closed-loop poles at 0 and -2 ?

1. $\mathbf{K} = [1 \ 2]$
2. $\mathbf{K} = [3 \ 4]$
3. $\mathbf{K} = \begin{bmatrix} 1 \\ 2 \end{bmatrix}$
4. $\mathbf{K} = \begin{bmatrix} 3 \\ 4 \end{bmatrix}$
5. none of the above

Check Yourself

$$\mathbf{A} = \begin{bmatrix} 1 & 1 \\ 0 & 1 \end{bmatrix} \quad \mathbf{B} = \begin{bmatrix} 0 \\ 1 \end{bmatrix}$$

Find \mathbf{K} so that the closed-loop poles are at 0 and -2 .

$$\begin{aligned} |s\mathbf{I} - (\mathbf{A} - \mathbf{BK})| &= \left| \begin{bmatrix} s-1 & -1 \\ k_1 & s+k_2-1 \end{bmatrix} \right| = (s-1)(s+k_2-1) + k_1 \\ &= s^2 + (k_2-2)s + k_1 - k_2 + 1 \\ &= s(s+2) = s^2 + 2s \end{aligned}$$

$$k_2 - 2 = 2$$

$$k_1 - k_2 + 1 = 0$$

Solving, we find $k_2 = 4$ and $k_1 = 3$.

Check Yourself

Let \mathbf{A} represent the system matrix and \mathbf{B} represent the input matrix for a state-space control system, where these matrices are given by

$$\mathbf{A} = \begin{bmatrix} 1 & 1 \\ 0 & 1 \end{bmatrix} \quad \mathbf{B} = \begin{bmatrix} 0 \\ 1 \end{bmatrix}$$

Which \mathbf{K} vector will produce closed-loop poles at 0 and -2 ? **2.**

1. $\mathbf{K} = [1 \ 2]$
2. $\mathbf{K} = [3 \ 4]$
3. $\mathbf{K} = \begin{bmatrix} 1 \\ 2 \end{bmatrix}$
4. $\mathbf{K} = \begin{bmatrix} 3 \\ 4 \end{bmatrix}$
5. none of the above

Pole Placement

With full-state feedback, the gains \mathbf{K} can be adjusted to produce **ANY** set of n closed-loop poles! → **much more powerful than classical methods!**

The design problem shifts ...

- from finding gains to optimize pole locations (classical view)
- to finding pole locations to optimize performance (modern view).

Examples: Next Lecture