# 6.3100: Dynamic System Modeling and Control Design

**Frequency Response and Bode Diagrams** 

March 13, 2024

#### **Retrospective: Eigenfunctions and Eigenvalues**

If a system contains only adders, gains, differentiators, and integrators, then its system function can be written as a **rational polynomial** in s:

$$H(s) = \frac{Y}{X}$$

The eigenfunctions of such systems are **complex exponentials**  $(e^{s_0t})$  and associated eigenvalues are given by the system function evaluated at  $s_0$ .



#### **Retrospective: Frequency Response**

The response of such a system to a sinusoidal input is determined by its system function H(s) evaluated at  $s=j\omega_0$ .

$$e^{j\omega_0 t} \to H(j\omega_0)e^{j\omega_0 t}$$

$$e^{-j\omega_0 t} \to H(-j\omega_0)e^{-j\omega_0 t}$$

$$\cos(\omega_0 t) = \frac{1}{2} \left( e^{j\omega_0 t} + e^{-j\omega_0 t} \right) \to \frac{1}{2} \left( H(j\omega_0)e^{j\omega_0 t} + H(-j\omega_0)e^{-j\omega_0 t} \right)$$

$$\to \operatorname{Re} \left( H(j\omega_0)e^{j\omega_0 t} \right)$$

$$\to \operatorname{Re} \left( |H(j\omega_0)|e^{j\angle H(j\omega_0)}e^{j\omega_0 t} \right)$$

$$\to |H(j\omega_0)| \operatorname{Re} \left( e^{j\angle H(j\omega_0)+j\omega_0 t} \right)$$

$$\to |H(j\omega_0)| \cos(\omega_0 t + \angle H(j\omega_0))$$

$$\cos(\omega_0 t) \longrightarrow H(s)\Big|_{s=j\omega_0} \longrightarrow |H(j\omega_0)|\cos(\omega_0 t + \angle H(j\omega_0))$$

#### **Retrospective:** Poles and Zeros

If a system contains only adders, gains, differentiators, and integrators, then its system function can be written as a **rational polynomial** in *s*:

$$H(s) = \frac{b_0 + b_1 s + b_2 s^2 + b_3 s^3 + \cdots}{a_0 + a_1 s + a_2 s^2 + a_3 s^3 + \cdots}$$

The numerator and denominator polynomials can be factored into products of terms: one for each **zero** in the numerator or **pole** in the denominator:

$$H(s) = K \frac{(s - z_0)(s - z_1)(s - z_2) \cdots}{(s - p_0)(s - p_1)(s - p_2) \cdots}$$

Even a complicated system is completely described by a small number of constants: K,  $z_0$ ,  $p_0$ ,  $z_1$ ,  $p_1$ ,  $z_2$ ,  $p_2$ ,...

#### Vector Interpretation of the Frequency Response

The frequency response of a system is determined by the ratio of the product of vectors from each zero to the point  $j\omega_0$  divided by the product of vectors from each pole to the point  $j\omega_0$ .

$$H(j\omega_0) = K \frac{(j\omega_0 - z_0)(j\omega_0 - z_1)(j\omega_0 - z_2)\cdots}{(j\omega_0 - p_0)(j\omega_0 - p_1)(j\omega_0 - p_2)\cdots}$$



While this approach is simple (compared to solving a differential equation), using **Bode Diagrams** is even simpler.



















Two asymptotes provide a good approximation on log-log axes.



 $\lim_{\omega\to\infty}|H(j\omega)|=\omega$ 





















Two asymptotes provide a good approximation on log-log axes.



# **Check Yourself**

Compare log-log plots of the frequency-response magnitudes of the following system functions:

$$H_1(s) = \frac{1}{s+1}$$
 and  $H_2(s) = \frac{1}{s+10}$ 

The former can be transformed into the latter by

- 1. shifting horizontally
- 2. shifting and scaling horizontally
- 3. shifting both horizontally and vertically
- 4. shifting and scaling both horizontally and vertically
- 5. none of the above

#### **Check Yourself**

Compare log-log plots of the frequency-response magnitudes of the following system functions:

$$H_{1}(s) = \frac{1}{s+1} \quad \text{and} \quad H_{2}(s) = \frac{1}{s+10}$$

$$\log |H(j\omega)|$$

$$-1$$

$$-2$$

$$-2$$

$$-1$$

$$0$$

$$1$$

$$H_{1}(j\omega)|$$

$$H_{1}(j\omega)|$$

$$H_{1}(j\omega)|$$

$$-1$$

$$H_{2}(j\omega)|$$

$$H_{2}($$

# **Check Yourself**

Compare log-log plots of the frequency-response magnitudes of the following system functions:

$$H_1(s) = \frac{1}{s+1}$$
 and  $H_2(s) = \frac{1}{s+10}$ 

The former can be transformed into the latter by 3

- 1. shifting horizontally
- 2. shifting and scaling horizontally
- 3. shifting both horizontally and vertically
- 4. shifting and scaling both horizontally and vertically
- 5. none of the above

no scaling in either vertical or horizontal directions!

# Asymptotic Behavior of More Complicated Systems

Constructing  $H(s_0)$ .

$$H(s_0) = K \quad \frac{\prod_{q=1}^Q (s_0 - z_q)}{\prod_{p=1}^P (s_0 - p_p)} \quad \leftarrow \text{ product of vectors for zeros}$$



#### Asymptotic Behavior of More Complicated Systems

The magnitude of a product is the product of the magnitudes.

$$|H(s_0)| = \left| K \quad \frac{\prod_{q=1}^{Q} (s_0 - z_q)}{\prod_{p=1}^{P} (s_0 - p_p)} \right| = |K| \quad \frac{\prod_{q=1}^{Q} |s_0 - z_q|}{\prod_{p=1}^{P} |s_0 - p_p|}$$



# **Bode Plot**

The log of the magnitude is a sum of logs.

$$|H(s_0)| = \left| K \quad \frac{\prod_{q=1}^{Q} (s_0 - z_q)}{\prod_{p=1}^{P} (s_0 - p_p)} \right| = |K| \quad \frac{\prod_{q=1}^{Q} |s_0 - z_q|}{\prod_{p=1}^{P} |s_0 - p_p|}$$

$$\log |H(j\omega)| = \log |K| + \sum_{q=1}^{Q} \log |j\omega - z_q| - \sum_{p=1}^{P} \log |j\omega - p_p|$$










# Asymptotic Behavior: Single Zero

Three straight lines provide a good approximation versus log  $\omega$ .



#### Asymptotic Behavior: Single Pole

The angle response is simple at low and high frequencies.



### Asymptotic Behavior: Single Pole

Three straight lines provide a good approximation versus log  $\omega$ .



The angle of a product is the sum of the angles.

$$\angle H(s_0) = \angle \left( K \frac{\prod_{q=1}^{Q} (s_0 - z_q)}{\prod_{p=1}^{P} (s_0 - p_p)} \right) = \angle K + \sum_{q=1}^{Q} \angle (s_0 - z_q) - \sum_{p=1}^{P} \angle (s_0 - p_p)$$



The angle of K can be 0 or  $\pi$ .









#### From Frequency Response to Bode Plot

The magnitude of  $H(j\omega)$  is a product of magnitudes.

$$|H(j\omega)| = |K| \frac{\prod_{q=1}^{Q} |j\omega - z_q|}{\prod_{p=1}^{P} |j\omega - p_p|}$$

 $\cap$ 

The log of the magnitude is a sum of logs.

$$\log |H(j\omega)| = \log |K| + \sum_{q=1}^{Q} \log |j\omega - z_q| - \sum_{p=1}^{P} \log |j\omega - p_p|$$

The angle of  $H(j\omega)$  is a sum of angles.

$$\angle H(j\omega) = \angle K + \sum_{q=1}^{Q} \angle (j\omega - z_q) - \sum_{p=1}^{P} \angle (j\omega - p_p)$$



5. none of the above



5. none of the above









# **Bode Plot: Accuracy**

The straight-line approximations are surprisingly accurate.



#### **Complex-Valued Poles and Zeros**

New issues arise for complex-valued poles and zeros.

We have previously seen that complex-valued poles are associated with **resonance**. How does resonance affect a Bode plot?

The frequency-response magnitude of a high-Q system is peaked.

Q = 0.501





$$Q = 2$$

$$H(s) = \frac{1}{1 + \frac{1}{Q} \frac{s}{\omega_0} + \left(\frac{s}{\omega_0}\right)^2}$$

$$\int_{-1}^{\frac{s}{\omega_0} \text{ plane}} \sqrt{1 - \left(\frac{1}{2Q}\right)^2} \int_{-1}^{\log |H(j\omega)|} \sqrt{1 - \left(\frac{1}{2Q}\right)^2} \int_{-2}^{-1} \int_{-1}^{-1} \int_{-1$$

$$Q = 4$$

$$H(s) = \frac{1}{1 + \frac{1}{Q}\frac{s}{\omega_0} + \left(\frac{s}{\omega_0}\right)^2}$$

$$\stackrel{s}{\longrightarrow} \text{plane} \sqrt{1 - \left(\frac{1}{2Q}\right)^2} 0 \frac{\log|H(j\omega)|}{-1 - \frac{1}{2Q}} - \frac{1}{2Q} - \frac{1}{2Q}$$

$$Q = 8$$

$$H(s) = \frac{1}{1 + \frac{1}{Q}\frac{s}{\omega_0} + \left(\frac{s}{\omega_0}\right)^2}$$

$$\int_{-1}^{\frac{s}{\omega_0}} \frac{|\log |H(j\omega)|}{\sqrt{1 - \left(\frac{1}{2Q}\right)^2}} \int_{-1}^{\log |H(j\omega)|} \int_{-1}^{\frac{1}{2Q}} \int_{-1}^{-1} \int_{-\frac{1}{2Q}} \int_{-2}^{-1} \int_{-1}^{-1} \int_{-\frac{1}{2Q}} \int_{-2}^{-1} \int_{-1}^{-1} \int_{-\frac{1}{2Q}} \int_{-2}^{-1} \int_{-1}^{-1} \int_{-\frac{1}{2Q}} \int_{-2}^{-1} \int_{-1}^{-1} \int_{-\frac{1}{2Q}} \int_{-\frac{1}{2}} \int_{-\frac{1}$$



As Q increases, the phase changes more abruptly with  $\omega.$ 

Q=0.501

As Q increases, the phase changes more abruptly with  $\omega.$ 

Q = 1

As Q increases, the phase changes more abruptly with  $\omega.$ 

$$Q=2$$

$$H(s) = \frac{1}{1 + \frac{1}{Q}\frac{s}{\omega_0} + \left(\frac{s}{\omega_0}\right)^2}$$



As Q increases, the phase changes more abruptly with  $\omega.$ 

$$Q = 4$$

$$H(s) = \frac{1}{1 + \frac{1}{Q}\frac{s}{\omega_0} + \left(\frac{s}{\omega_0}\right)^2}$$



As Q increases, the phase changes more abruptly with  $\omega.$ 

$$Q=8$$

$$H(s) = \frac{1}{1 + \frac{1}{Q}\frac{s}{\omega_0} + \left(\frac{s}{\omega_0}\right)^2}$$









5.  $\omega_r < \omega_d$ 

# Check Yourself: Frequency Response

Analyze with vectors.



The product of the lengths is  $\left(\sqrt{(\omega_r + \omega_d)^2 + \sigma^2}\right)\left(\sqrt{(\omega_d - \omega_r)^2 + \sigma^2}\right)$ .

# Check Yourself: Frequency Response

Analyze with vectors.



The product of the lengths is  $\left(\sqrt{(\omega_r + \omega_d)^2 + \sigma^2}\right)\left(\sqrt{(\omega_d - \omega_r)^2 + \sigma^2}\right)$ . Decreasing  $\omega_r$  from  $\omega_d$  to  $\omega_d - \epsilon$  decreases the product since length of

bottom vector decreases as  $\epsilon$  while length of top vector increases only as  $\epsilon^2$ .

# Check Yourself: Frequency Response

More mathematically ...



The product of the lengths is  $\left(\sqrt{(\omega_r + \omega_d)^2 + \sigma^2}\right) \left(\sqrt{(\omega_r - \omega_d)^2 + \sigma^2}\right)$ .

Maximum occurs where derivative of squared lengths is zero.

$$\frac{d}{d\omega_r}\left((\omega_r + \omega_d)^2 + \sigma^2\right)\left((\omega_r - \omega_d)^2 + \sigma^2\right) = 0$$

 $\label{eq:constraint} \rightarrow \quad \omega_r^2 = \omega_d^2 - \sigma^2 = \omega_0^2 - 2\sigma^2 \, .$ 



5.  $\omega_r < \omega_d$ 






5.  $\omega < \omega_d$ 

The phase is 0 when  $\omega = 0$ .



The phase hasn't reached  $-\pi/2$  when  $\omega = \omega_d$ .



The phase is  $-\pi/2$  at  $\omega = \omega_0$ .





5.  $\omega < \omega_d$ 

#### Summary

The frequency response of a system is easily determined using Bode plots.

Each pole and each zero contributes one section to the Bode plot.

The magnitude of the response of the system is given by the sum of the log magnitudes for the sections contributed by each pole and zero.

The angle of the response of the system is given by the sum of the angles for the sections contributed by each pole and zero.